

Wilson's Corners N.

Auburn Township

111

DIETZGEN
D.   TRADE MARK

ENGINEERS'

LEVEL BOOK

No. 410

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

PLEASE RETURN TO
DISTANCE FROM CENTER OF ROADWAY FOR CROSS SECTIONING
FOR SINGLE TRACK RAILROADS

GAUGA COUNTY ENGINEER

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 - (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.

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Messenger Road - No. 31
Sections A B & C

X-Sections - pg. - 3-29
Slope Stakes - pg. - 30
CULVERTS - Pg. - 65

Messenger Road
Ditch
Levels E & W ± 1350.0 's of Franks Rd
To Cross Culvt.

1957 - 24
1974 - 25

111

State Road 35 (U.S. 422)

B.M. Nail in Locust Stump

* Sta. 430 ± Elev. 1272.44

B.M. Notch in Maple Sta 425 ±

Elev. 1238.56

B.M. Nail in Root 24" Chestnut

Sta 421 ± Elev. 1215.26

B.M. Notch in Maple Sta 444 ± 90

* Elev. 1278.94

I.C.H. 324. State Route 44

* B.M. Sta 144+18 Roofing nail in s.e.

Root 18" Maple Stump 30' Lt.

Elev. 1219.58

Note: * indicates B.M. found
& Used.

B.M.s Copied from State Plans.

Wilson's Corners N.

BENCH MARKS

B.M.#1 Nail in West Root 30" Maple

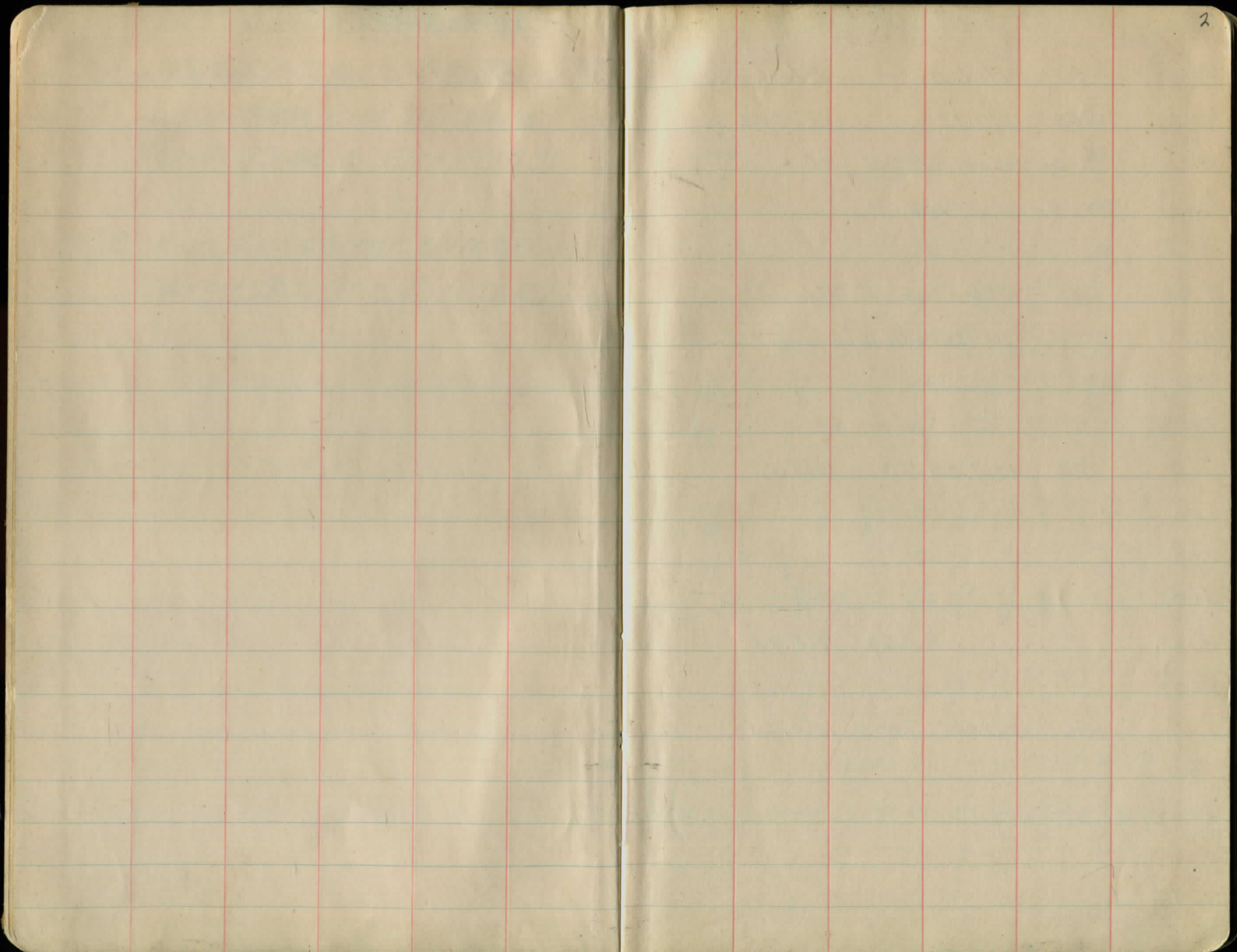
Sta 5+73.55 E. Elev. 1263.98

B.M.#2 X on S.W. Corner E. Headwall

Culvert Sta 19+ E. 1221.075

Wilson's Corners N.

BENCH MARKS



Sta	+	H.I.	Elev.	Rem.
10+0		1262.085		
10+50				
T.P.	8.495	1254.880	10.70	1251.385
11+0				
+50				
T.P.	2.34	1245.61	11.61	1243.27
12+0				
+50				
13+0				
T.P.	1.15	1239.785	12.975	1232.635
13+90				
14+0				
15+0				
16+0				
T.P.	2.335	1223.790	12.33	1221.455
17+0				
18+0				
19+0				
+30.9		CULVERT		
B.M.		2.80	1220.99	

E.											W	4	
$\frac{6.0}{25}$	$\frac{5.2}{23}$	$\frac{5.9}{17}$	$\frac{8.2}{10}$	$\frac{7.2}{10}$	$\frac{6.7}{7}$	$\frac{6.5}{7}$	$\frac{6.8}{7}$	$\frac{7.6}{9}$	$\frac{6.0}{12}$	$\frac{5.0}{14}$	$\frac{5.1}{25}$		
$\frac{7.9}{25}$	$\frac{7.7}{18}$	$\frac{9.5}{15}$	$\frac{11.2}{11}$	$\frac{9.5}{7}$	$\frac{9.4}{7}$	$\frac{9.4}{7}$	$\frac{10.5}{10}$	$\frac{8.5}{13}$	$\frac{6.6}{16}$	$\frac{6.9}{25}$			
$\frac{3.2}{25}$	$\frac{3.2}{20}$	$\frac{7.2}{12}$	$\frac{5.7}{8}$	$\frac{5.4}{8}$	$\frac{5.4}{8}$	$\frac{6.0}{10}$	$\frac{4.4}{13}$	$\frac{0.8}{20}$	$\frac{0.6}{25}$				
$\frac{6.6}{25}$	$\frac{6.5}{19}$	$\frac{10.0}{12}$	$\frac{9.1}{9}$	$\frac{8.9}{9}$	$\frac{8.8}{7}$	$\frac{9.4}{9}$	$\frac{5.5}{17}$	$\frac{5.2}{24}$	$\frac{5.2}{25}$				
$\frac{0.3}{25}$	$\frac{0.5}{22}$	$\frac{2.7}{15}$	$\frac{3.1}{12}$	$\frac{2.9}{10}$	$\frac{3.0}{5}$	$\frac{3.3}{9}$	$\frac{3.3}{9}$	$\frac{1.1}{16}$	$\frac{1.3}{25}$				
$\frac{3.5}{33}$	$\frac{2.9}{21}$	$\frac{3.3}{21}$	$\frac{7.7}{16}$	$\frac{9.0}{14}$	$\frac{6.7}{9}$	$\frac{6.2}{8}$	$\frac{6.5}{7}$	$\frac{6.9}{9}$	$\frac{6.2}{13}$	$\frac{4.2}{13}$	$\frac{4.6}{25}$		
$\frac{7.3}{25}$	$\frac{8.4}{28}$	$\frac{10.9}{19}$	$\frac{12.8}{14}$	$\frac{11.6}{10}$	$\frac{11.0}{10}$	$\frac{11.1}{5}$	$\frac{11.9}{7}$	$\frac{8.3}{13}$	$\frac{7.8}{25}$				
$\frac{4.2}{25}$	$\frac{4.6}{21}$	$\frac{5.8}{17}$	$\frac{7.3}{14}$	$\frac{6.3}{13}$	$\frac{5.9}{10}$	$\frac{6.1}{10}$	$\frac{6.2}{4}$	$\frac{7.1}{6}$	$\frac{6.0}{8}$	$\frac{6.0}{19}$	$\frac{6.4}{24}$	$\frac{6.4}{25}$	
$\frac{5.3}{25}$	$\frac{5.8}{22}$	$\frac{6.2}{17}$	$\frac{7.5}{14}$	$\frac{6.9}{13}$	$\frac{6.4}{10}$	$\frac{6.6}{10}$	$\frac{6.6}{4}$	$\frac{7.5}{6}$	$\frac{6.7}{8}$	$\frac{6.9}{15}$	$\frac{7.3}{22}$	$\frac{7.5}{25}$	
$\frac{8.8}{25}$	$\frac{9.4}{21}$	$\frac{10.0}{15}$	$\frac{11.6}{11}$	$\frac{10.2}{9}$	$\frac{10.2}{9}$	$\frac{10.2}{9}$	$\frac{10.2}{4}$	$\frac{10.8}{6}$	$\frac{10.3}{8}$	$\frac{10.9}{14}$	$\frac{11.6}{20}$	$\frac{11.8}{25}$	
$\frac{12.7}{25}$	$\frac{12.7}{21}$	$\frac{12.3}{16}$	$\frac{13.3}{13}$	$\frac{12.3}{10}$	$\frac{12.3}{10}$	$\frac{12.3}{10}$	$\frac{12.4}{4}$	$\frac{12.9}{6}$	$\frac{12.5}{9}$	$\frac{13.0}{10}$	$\frac{13.7}{16}$	$\frac{14.6}{25}$	
$\frac{3.4}{25}$	$\frac{3.6}{20}$	$\frac{4.1}{15}$	$\frac{4.5}{12}$	$\frac{3.9}{9}$	$\frac{3.6}{3}$	$\frac{3.2}{3}$	$\frac{4.0}{4}$	$\frac{4.2}{6}$	$\frac{4.0}{7}$	$\frac{4.7}{10}$	$\frac{5.2}{25}$		
$\frac{4.8}{25}$	$\frac{4.9}{22}$	$\frac{4.5}{17}$	$\frac{5.3}{14}$	$\frac{4.7}{12}$	$\frac{4.4}{4}$	$\frac{4.6}{4}$	$\frac{5.0}{4}$	$\frac{5.2}{6}$	$\frac{4.9}{8}$	$\frac{4.8}{14}$	$\frac{4.8}{25}$		
$\frac{5.2}{25}$	$\frac{5.1}{22}$	$\frac{6.6}{20}$	$\frac{5.4}{18}$	$\frac{4.6}{16}$	$\frac{4.4}{6}$	$\frac{4.6}{6}$	$\frac{4.9}{2}$	$\frac{5.3}{4}$	$\frac{5.8}{5}$	$\frac{5.2}{7}$	$\frac{5.8}{10}$	$\frac{6.2}{25}$	
(W	$\frac{8.2}{5.1}$	$\frac{2.9}{5}$	$\frac{4.1}{2}$	$\frac{4.0}{2}$	$\frac{3.8}{8}$	$\frac{4.0}{15}$	$\frac{2.8}{15}$	$\frac{8.0}{15}$	$\frac{6.7}{25}$	E)			

Sta + H. I. 1223.79 Elev. Rem. E

20+0

21+0

T.P. 11.54 1234.40 0.93 1222.86

21+28

21+65 Love's House W. side of Rd.

22+0 E of Drive W. side of Rd.

22+34 Bag of Bark on E. side of Rd.

T.P. 6.865 1238.935 2.33 1232.07

23+0

23+39

24+0

25+0

26+0

T.P. 12.315 1241.915 9.335 1229.600

6

4.7	4.5	3.9	4.7	4.1	3.8	4.3	4.5	4.9	4.3	4.7	5.3	5.7	
25	21	19	17	16	7		1	2	4	6	19	25	
		1.0	1.6	2.1	1.7	1.5	1.9	2.1	1.4	0.7	0.3	0.4	0.5
		25	18	15	14	6		1	2	5	12	13	25

8.4	9.5	10.2	11.2	10.8	11.5	11.7	11.0	9.8	9.1	8.8		
54	25	19	15	8		1	2	7	12	25		
6.5	7.3	8.3	8.2	8.1	9.0	9.0	8.7	8.0	8.2	8.0	6.8	
25	20	17	15	9		1	4	7	19	25	84 House	

5.9	6.5	7.0	6.8	6.6	7.1	7.0	7.0	7.2	7.3		
25	20	16	14	9		3	7	18	25		

0.9	1.4	4.2	5.3	5.7	5.5	5.6	5.6	5.4	5.8	5.8	
26	25	21	18	15	8		4	7	16	25	

0.2	1.8	7.1	7.5	7.0	6.5	7.0	7.2	7.9	7.6	8.2	9.1
29	25	17	15	13	7		2	5	6	16	25

5.0	1.4	5.6	6.1	5.5	4.7	5.1	5.6	6.2	6.0	7.3	8.7	10.0	10.3
FR.	25	19	15	13	6		3	5	7	15	25	42	45

2.1	1.9	5.5	6.2	5.7	5.1	5.9	6.5	7.1	6.9	8.4	9.3	
30	24	19	15	13	7		2	4	6	18	25	

9.6	9.4	9.3	8.9	9.0	8.7	9.3	9.4	10.0	9.5	9.5	10.0	
27	25	21	16	15	7		2	3	5	17	25	

10.1	10.3	9.7	9.3	9.6	10.0	10.7	10.2	10.7	10.8		
25	20	14	5		4	5	7	17	25		

34a

+

H.I.
1246.715

Elev. Rem.

27+0

28+0

29+0

29+18

T.P. 8.12 1246.89 3.145 1238.770

B.M. 3.63 1243.265

E.

E

W.

6

$\frac{9.8}{25}$	$\frac{9.9}{14}$	$\frac{11.7}{11}$	$\frac{12.7}{10}$	$\frac{12.0}{7}$	11.8	$\frac{11.8}{5}$	$\frac{12.2}{7}$	$\frac{11.3}{8}$	$\frac{10.4}{25}$
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$\frac{9.9}{25}$	$\frac{9.8}{24}$	$\frac{10.5}{17}$	$\frac{10.4}{10}$	$\frac{11.1}{9}$	$\frac{10.1}{7}$	10.1	$\frac{10.4}{7}$	$\frac{11.0}{8}$	$\frac{10.7}{10}$	$\frac{11.3}{15}$	$\frac{11.7}{25}$
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$\frac{8.4}{25}$	$\frac{8.0}{18}$	$\frac{8.2}{11}$	$\frac{8.5}{9}$	$\frac{8.3}{7}$	8.2	$\frac{8.2}{6}$	$\frac{8.0}{7}$	$\frac{8.8}{8}$	$\frac{8.4}{9}$	$\frac{8.1}{20}$	$\frac{7.8}{25}$
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$\frac{7.0}{25}$	$\frac{7.0}{14}$	$\frac{7.3}{11}$	$\frac{7.9}{9}$	$\frac{7.6}{7}$	$\frac{7.1}{2}$	7.1	$\frac{7.4}{6}$	$\frac{8.0}{7}$	$\frac{7.0}{9}$	$\frac{5.6}{15}$	$\frac{5.0}{22}$	$\frac{5.1}{25}$
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JUNE 8, 1929 Fair. 5 Gold
S. Merritt
H. Barton

E.

±

W.

7

Sta + H.I. - Elev. Remis

B.M. 3.31 1246.57 1243.26 Nail in

30+0 N.E. Roof
18" Mark
Sta 29+90

$\frac{4.8}{25}$ $\frac{4.1}{22}$ $\frac{4.3}{18}$ $\frac{4.5}{12}$ $\frac{5.3}{10}$ $\frac{7.1}{7}$ $\frac{6.9}{5}$ 6.6 $\frac{6.8}{4}$ $\frac{7.2}{7}$ $\frac{5.5}{10}$ $\frac{4.1}{14}$ $\frac{3.7}{20}$ $\frac{3.6}{25}$

31+0

$\frac{1.5}{25}$ $\frac{1.4}{22}$ $\frac{1.6}{15}$ $\frac{2.1}{9}$ $\frac{2.7}{7}$ $\frac{3.8}{5}$ $\frac{3.7}{4}$ 3.4 $\frac{3.2}{3}$ $\frac{3.7}{10}$ $\frac{4.2}{11}$ $\frac{3.4}{13}$ $\frac{3.2}{17}$ $\frac{4.1}{25}$

32+0

$\frac{7.3}{25}$ $\frac{7.3}{18}$ $\frac{7.1}{12}$ $\frac{6.5}{7}$ $\frac{6.7}{5}$ $\frac{6.1}{3}$ 6.0 $\frac{5.9}{3}$ $\frac{5.8}{11}$ $\frac{6.5}{15}$ $\frac{6.8}{22}$ $\frac{6.8}{25}$

33+0

$\frac{2.8}{25}$ $\frac{2.7}{20}$ $\frac{2.7}{17}$ $\frac{3.5}{8}$ $\frac{5.3}{4}$ 4.9 $\frac{4.5}{4}$ $\frac{5.1}{10}$ $\frac{5.4}{12}$ $\frac{4.7}{15}$ $\frac{5.3}{25}$

T.P. 1.44 1244.94 3.07 1243.50

33+36 ± of Drive E. side

$\frac{0.4}{25}$ $\frac{0.7}{20}$ $\frac{1.3}{9}$ $\frac{2.3}{4}$ 2.1

34+0

$\frac{0.2}{25}$ $\frac{0.9}{16}$ $\frac{1.7}{7}$ $\frac{2.7}{4}$ 2.4 $\frac{2.2}{4}$ $\frac{2.5}{9}$ $\frac{2.9}{13}$ $\frac{2.6}{17}$ $\frac{2.6}{25}$

35+0

$\frac{3.0}{25}$ $\frac{3.6}{21}$ $\frac{4.3}{18}$ $\frac{5.1}{13}$ $\frac{5.2}{7}$ $\frac{4.9}{5}$ 4.5 $\frac{4.4}{2}$ $\frac{5.0}{9}$ $\frac{5.8}{10}$ $\frac{5.5}{12}$ $\frac{5.5}{16}$ $\frac{5.7}{25}$

35+54 ± of 12" Tile

$\frac{7.1}{25}$ $\frac{7.2}{28}$ $\frac{7.6}{F.L.}$ $\frac{5.7}{6}$ 5.0 $\frac{5.6}{6}$ $\frac{7.4}{F.L.}$ $\frac{7.6}{11}$

36+0

$\frac{6.6}{25}$ $\frac{6.2}{19}$ $\frac{5.2}{11}$ $\frac{5.6}{9}$ $\frac{5.1}{5}$ 5.1 $\frac{5.1}{5}$ $\frac{5.4}{8}$ $\frac{5.4}{14}$ $\frac{4.7}{18}$ $\frac{4.1}{25}$

Sta + Elev. Rem's

14
124494

37+0

T.P. 11.66 1255.35 1.25 1243.69

38+0

39+0

40+0

40+24

41+0

41+35

42+0

42+30

43+0

E

W 8

$\frac{5.2}{25}$ $\frac{4.9}{19}$ $\frac{4.1}{12}$ $\frac{4.3}{8}$ $\frac{3.7}{6}$ 3.6 $\frac{4.1}{5}$ $\frac{4.5}{8}$ $\frac{4.7}{12}$ $\frac{5.0}{19}$ $\frac{5.2}{25}$

$\frac{9.0}{25}$ $\frac{9.5}{20}$ $\frac{11.0}{12}$ $\frac{11.3}{12}$ $\frac{12.3}{9}$ $\frac{11.3}{8}$ $\frac{10.7}{2}$ 10.8 $\frac{11.3}{4}$ $\frac{11.5}{6}$ $\frac{10.8}{9}$ $\frac{10.8}{13}$ $\frac{10.9}{25}$

$\frac{6.9}{25}$ $\frac{7.8}{21}$ $\frac{8.6}{15}$ $\frac{8.5}{12}$ $\frac{9.1}{9}$ $\frac{8.8}{7}$ $\frac{8.7}{7}$ 8.7 $\frac{8.8}{5}$ $\frac{9.2}{7}$ $\frac{8.9}{10}$ $\frac{8.6}{25}$

$\frac{2.8}{28}$ $\frac{3.2}{22}$ $\frac{4.0}{17}$ $\frac{5.3}{15}$ $\frac{5.4}{12}$ $\frac{6.3}{10}$ $\frac{6.0}{9}$ 5.5 $\frac{6.1}{5}$ $\frac{6.4}{6}$ $\frac{5.2}{9}$ $\frac{5.4}{17}$ $\frac{5.3}{25}$

$\frac{3.2}{25}$ $\frac{4.0}{17}$ $\frac{5.1}{12}$ $\frac{5.7}{10}$ $\frac{5.3}{9}$ 4.6 $\frac{5.4}{6}$ $\frac{5.7}{8}$ $\frac{5.1}{10}$ $\frac{5.2}{25}$

$\frac{3.4}{25}$ $\frac{3.8}{19}$ $\frac{4.7}{12}$ $\frac{5.5}{10}$ $\frac{4.5}{8}$ 4.2 $\frac{4.7}{6}$ $\frac{5.2}{8}$ $\frac{5.6}{17}$ $\frac{5.8}{25}$

$\frac{3.0}{25}$ $\frac{3.2}{20}$ $\frac{4.1}{14}$ $\frac{5.6}{10}$ $\frac{4.7}{8}$ 4.0 $\frac{4.6}{6}$ $\frac{5.4}{9}$ $\frac{5.3}{16}$ $\frac{5.5}{25}$

$\frac{3.2}{25}$ $\frac{4.2}{19}$ $\frac{4.8}{14}$ $\frac{6.5}{11}$ $\frac{5.7}{8}$ 5.3 $\frac{5.9}{7}$ $\frac{6.2}{8}$ $\frac{6.1}{11}$ $\frac{6.6}{23}$ $\frac{7.0}{25}$

$\frac{4.2}{25}$ $\frac{5.4}{18}$ $\frac{6.6}{13}$ $\frac{5.8}{10}$ 5.9 $\frac{5.8}{3}$ $\frac{6.1}{10}$ $\frac{6.7}{18}$ $\frac{7.2}{25}$

$\frac{5.9}{25}$ $\frac{6.2}{19}$ $\frac{7.1}{17}$ $\frac{6.6}{16}$ $\frac{6.2}{13}$ $\frac{5.3}{11}$ 5.2 $\frac{5.3}{6}$ $\frac{6.6}{8}$ $\frac{7.2}{12}$ $\frac{7.5}{23}$ $\frac{7.6}{25}$

Sta + H.I. - Elev. Rem's

1255.35

43+23 $\frac{1}{2}$ of Stone Culvert.

B.M. S.T.P. 7.60 1259.75 3.20 1252.15

44+0 House on W. Side

44+65 $\frac{1}{2}$ of Drive on W. Side

45+0

46+0

T.P. 9.13 1267.98 0.90 1258.85

47+0

48+0

49+0

50+0

T.P. 2.06 1264.85 5.19 1262.79

51+0

E.

$\frac{1}{2}$

W

9

$\frac{8.2}{15}$ $\frac{8.6}{F.L.}$ $\frac{3.2}{11}$ $\frac{4.2}{11}$ 4.8 $\frac{4.6}{5}$ $\frac{3.3}{5}$ $\frac{8.8}{F.L.}$ $\frac{9.0}{25}$

$\frac{6.8}{25}$ $\frac{6.9}{23}$ $\frac{8.3}{20}$ $\frac{8.5}{12}$ $\frac{8.0}{12}$ $\frac{7.8}{3}$ 8.0 $\frac{8.2}{2}$ $\frac{7.1}{10}$ $\frac{6.5}{18}$ $\frac{6.1}{25}$ $\frac{3.6}{HOUSE}$

5.1 $\frac{5.0}{4}$ $\frac{4.9}{9}$ $\frac{4.4}{25}$

$\frac{2.9}{25}$ $\frac{3.1}{18}$ $\frac{5.1}{12}$ $\frac{4.3}{10}$ $\frac{4.0}{5}$ 4.0 $\frac{4.2}{5}$ $\frac{4.6}{8}$ $\frac{3.7}{10}$ $\frac{3.3}{21}$ $\frac{3.1}{25}$

+02 $\frac{0.2}{25}$ $\frac{1.6}{13}$ $\frac{2.5}{11}$ $\frac{1.8}{9}$ 1.4 $\frac{2.1}{7}$ $\frac{2.7}{10}$ $\frac{1.8}{12}$ $\frac{1.7}{20}$ $\frac{2.0}{25}$

$\frac{4.3}{25}$ $\frac{4.7}{21}$ $\frac{6.0}{17}$ $\frac{2.6}{13}$ $\frac{7.6}{11}$ $\frac{6.9}{9}$ 6.4 $\frac{6.9}{6}$ $\frac{7.6}{8}$ $\frac{6.6}{10}$ $\frac{6.5}{16}$ $\frac{6.4}{21}$ $\frac{6.6}{25}$

$\frac{2.2}{25}$ $\frac{2.8}{20}$ $\frac{3.5}{14}$ $\frac{4.6}{10}$ $\frac{4.1}{7}$ 3.7 $\frac{4.3}{8}$ $\frac{5.1}{10}$ $\frac{4.6}{13}$ $\frac{4.7}{20}$ $\frac{4.6}{25}$

$\frac{3.0}{25}$ $\frac{3.5}{14}$ $\frac{3.8}{10}$ $\frac{4.7}{9}$ $\frac{4.3}{7}$ 4.1 $\frac{4.5}{7}$ $\frac{4.9}{10}$ $\frac{4.6}{12}$ $\frac{4.4}{25}$

$\frac{3.9}{25}$ $\frac{4.2}{18}$ $\frac{4.9}{11}$ $\frac{6.2}{9}$ $\frac{5.3}{6}$ 5.2 $\frac{5.1}{2}$ $\frac{5.7}{8}$ $\frac{6.1}{11}$ $\frac{6.1}{16}$ $\frac{6.0}{25}$

$\frac{2.2}{25}$ $\frac{2.4}{20}$ $\frac{3.1}{11}$ $\frac{4.8}{9}$ $\frac{3.5}{7}$ 3.1 $\frac{3.6}{8}$ $\frac{4.0}{10}$ $\frac{3.9}{14}$ $\frac{4.1}{25}$

549 + H.1. 126425 - Elev. Remas

52+0

53+0

54+0

55+0

56+0

T.P. 0.72 1258.82 6.75 1258.10

57+0

58+0

59+0

60+0

61+0

E.

E

W 10

 $\frac{2.8}{25}$ $\frac{2.9}{19}$ $\frac{3.2}{11}$ $\frac{4.9}{9}$ $\frac{4.2}{7}$ 3.6 $\frac{4.0}{7}$ $\frac{4.5}{10}$ $\frac{4.1}{12}$ $\frac{4.1}{18}$ $\frac{4.0}{25}$
 $\frac{5.0}{25}$ $\frac{4.6}{22}$ $\frac{5.1}{19}$ $\frac{5.1}{14}$ $\frac{5.7}{12}$ $\frac{4.7}{9}$ 4.2 $\frac{4.6}{8}$ $\frac{5.2}{10}$ $\frac{5.2}{12}$ $\frac{5.3}{21}$ $\frac{5.2}{25}$
 $\frac{5.4}{25}$ $\frac{5.0}{19}$ $\frac{5.1}{14}$ $\frac{5.9}{12}$ $\frac{5.3}{10}$ 4.9 $\frac{5.3}{7}$ $\frac{5.8}{10}$ $\frac{5.7}{14}$ $\frac{5.6}{18}$ $\frac{4.4}{21}$ $\frac{4.6}{25}$
 $\frac{6.3}{25}$ $\frac{6.5}{20}$ $\frac{6.7}{14}$ $\frac{7.1}{12}$ $\frac{6.2}{10}$ $\frac{5.7}{2}$ 5.8 $\frac{6.4}{6}$ $\frac{7.0}{8}$ $\frac{7.0}{12}$ $\frac{7.0}{22}$ $\frac{6.8}{25}$
 $\frac{6.5}{25}$ $\frac{6.8}{21}$ $\frac{7.1}{12}$ $\frac{7.6}{10}$ $\frac{6.7}{7}$ 6.2 $\frac{7.0}{8}$ $\frac{7.3}{9}$ $\frac{7.2}{11}$ $\frac{7.2}{21}$ $\frac{7.0}{25}$
 $\frac{1.1}{25}$ $\frac{1.2}{20}$ $\frac{1.6}{13}$ $\frac{2.8}{10}$ $\frac{1.8}{8}$ 1.2 $\frac{1.8}{8}$ $\frac{2.4}{7}$ $\frac{1.3}{12}$ $\frac{1.5}{19}$ $\frac{1.3}{25}$
 $\frac{2.5}{25}$ $\frac{2.9}{20}$ $\frac{3.7}{14}$ $\frac{5.2}{10}$ $\frac{4.1}{8}$ 3.3 $\frac{4.3}{8}$ $\frac{4.6}{9}$ $\frac{3.8}{11}$ $\frac{3.5}{18}$ $\frac{3.2}{25}$
 $\frac{5.5}{25}$ $\frac{5.7}{21}$ $\frac{5.9}{14}$ $\frac{7.1}{12}$ $\frac{6.0}{9}$ $\frac{5.2}{2}$ 5.4 $\frac{6.0}{6}$ $\frac{6.7}{8}$ $\frac{5.5}{10}$ $\frac{5.5}{17}$ $\frac{5.6}{25}$
 $\frac{7.3}{25}$ $\frac{7.4}{19}$ $\frac{7.4}{14}$ $\frac{8.3}{12}$ $\frac{7.6}{8}$ $\frac{7.1}{3}$ 7.2 $\frac{7.6}{5}$ $\frac{8.4}{7}$ $\frac{8.0}{9}$ $\frac{8.0}{16}$ $\frac{7.2}{23}$ $\frac{7.5}{25}$
 $\frac{8.4}{25}$ $\frac{8.7}{20}$ $\frac{8.5}{15}$ $\frac{10.0}{12}$ $\frac{8.8}{9}$ 8.6 $\frac{8.9}{6}$ $\frac{9.3}{7}$ $\frac{8.6}{9}$ $\frac{8.8}{14}$ $\frac{9.0}{20}$ $\frac{9.3}{25}$

Sta + H.I. - Elev. Rem's

1258.92

61+67 E of Drive on W. Side of Rd.

T.P. 2.55 1250.94 10.43 1248.39

62+0 House on West Side of Rd.

62+55

63+0

63+15

T.P. 2.76 1241.69 12.01 1238.95

B.M. 4.27 1237.42

X on S.M.
Cor. E.M.W.
DUMM
Sta 64

E. E. W. 11

10.6 $\frac{11.0}{7}$ $\frac{10.6}{8}$ $\frac{9.9}{14}$ $\frac{9.9}{18}$ $\frac{10.8}{25}$

$\frac{5.4}{18}$ $\frac{3.1}{15}$ $\frac{2.6}{13}$ $\frac{3.7}{12}$ $\frac{4.6}{10}$ $\frac{4.0}{8}$ 3.2 $\frac{4.2}{5}$ $\frac{2.8}{9}$ $\frac{2.6}{19}$ $\frac{2.7}{25}$ $\frac{2.7}{25}$ HOUSE

$\frac{2.2}{25}$ $\frac{2.6}{23}$

$\frac{4.9}{25}$ $\frac{5.3}{15}$ $\frac{7.6}{11}$ $\frac{7.9}{7}$ $\frac{7.0}{6}$ $\frac{6.7}{3}$ 6.9 $\frac{7.2}{5}$ $\frac{5.3}{8}$ $\frac{5.0}{26}$

$\frac{9.2}{25}$ $\frac{9.1}{21}$ $\frac{9.3}{15}$ $\frac{10.6}{13}$ $\frac{11.3}{10}$ $\frac{10.7}{8}$ $\frac{10.2}{3}$ 10.3 $\frac{10.7}{5}$ $\frac{11.4}{7}$ $\frac{9.0}{11}$ $\frac{7.1}{22}$ $\frac{6.7}{25}$

$\frac{10.2}{25}$ $\frac{11.1}{15}$ $\frac{12.1}{11}$ $\frac{11.2}{3}$ 11.3 $\frac{11.6}{5}$ $\frac{12.2}{7}$ $\frac{11.0}{10}$ $\frac{9.7}{15}$ $\frac{8.0}{23}$ $\frac{7.6}{25}$

June 10 - Clear

S. Gold St.
S. Morrison
H. Barton

Sta	+	H I	-	Elev.	Remarks
B.M.	0.62	1238.10		1237.42	1 on 55 Cor. E.H.W. Culvert. Sta 685
64+0					

+57± \neq Culvert
Note the water in the
Culvert runs into the ditch
along side of Rd.

65+0

66+0

67+0

T.P.	0.24	1226.75	11.59	1226.51	
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68+0

68+39± \neq of Culvert (12" C.I.P.)

69+0

69+55 Ditch running West

E

E

W. 17

$\frac{2.1}{25}$	$\frac{1.9}{21}$	$\frac{1.5}{14}$	$\frac{2.6}{11}$	$\frac{1.9}{8}$	1.4	$\frac{1.5}{5}$	$\frac{2.0}{7}$	$\frac{1.6}{9}$	$\frac{1.7}{18}$	$\frac{1.4}{25}$
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$\frac{5.1}{17}$	$\frac{5.9}{F.L.}$	$\frac{0.6}{10}$	$\frac{2.1}{10}$	2.4	$\frac{2.3}{7}$	$\frac{0.8}{7}$	$\frac{5.9}{F.L.}$	$\frac{5.5}{13}$	$\frac{4.9}{15}$
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$\frac{3.3}{25}$	$\frac{3.9}{22}$	$\frac{5.3}{14}$	$\frac{5.1}{16}$	$\frac{5.1}{12}$	5.0	$\frac{5.0}{2}$	$\frac{5.0}{4}$	$\frac{5.6}{7}$	$\frac{6.4}{8}$	$\frac{5.1}{11}$	$\frac{5.1}{12}$	$\frac{5.8}{25}$
------------------	------------------	------------------	------------------	------------------	-----	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{5.6}{25}$	$\frac{6.4}{16}$	$\frac{7.8}{11}$	$\frac{6.9}{9}$	$\frac{6.5}{4}$	6.8	$\frac{6.9}{2}$	$\frac{7.3}{6}$	$\frac{8.0}{9}$	$\frac{8.7}{10}$	$\frac{8.1}{12}$	$\frac{8.1}{18}$	$\frac{8.1}{25}$
------------------	------------------	------------------	-----------------	-----------------	-----	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.9}{25}$	$\frac{8.1}{21}$	$\frac{9.3}{18}$	$\frac{10.8}{14}$	$\frac{9.6}{12}$	$\frac{9.3}{7}$	$\frac{9.5}{2}$	10.2	$\frac{10.2}{2}$	$\frac{9.5}{4}$	$\frac{11.1}{6}$	$\frac{10.0}{8}$	$\frac{7.5}{15}$	$\frac{10.2}{25}$
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$\frac{1.8}{25}$	$\frac{0.7}{17}$	$\frac{1.4}{15}$	$\frac{2.5}{13}$	$\frac{2.1}{11}$	$\frac{1.6}{5}$	2.0	$\frac{2.7}{2}$	$\frac{1.5}{5}$	$\frac{2.2}{8}$	$\frac{3.1}{10}$	$\frac{0.8}{13}$	$\frac{1.1}{25}$
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$\frac{2.0}{17}$	$\frac{4.0}{F.L.}$	$\frac{2.9}{10}$	3.1	$\frac{3.5}{4}$	$\frac{5.1}{F.L.}$	$\frac{3.3}{11}$	$\frac{2.4}{10}$
------------------	--------------------	------------------	-----	-----------------	--------------------	------------------	------------------

$\frac{2.5}{25}$	$\frac{2.7}{20}$	$\frac{4.2}{15}$	$\frac{5.3}{13}$	$\frac{4.7}{11}$	$\frac{4.0}{4}$	4.5	$\frac{5.2}{6}$	$\frac{6.3}{9}$	$\frac{4.0}{12}$	$\frac{4.1}{25}$
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5.6	$\frac{5.9}{4}$	$\frac{5.1}{6}$	$\frac{6.7}{12}$	$\frac{7.1}{25}$	$\frac{7.1}{40}$	$\frac{7.7}{55}$
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Stn + Hgt. Elev. Rem's

122675

70+0

71+0

72+0

T.P. 3.32 1219.70 10.37 1216.38

73+0

74+0

74+36± E of Culvert (12" Tile)

75+0

76+0

+58 E of Drive E & W.

B.M. 0.5 1219.55

77+0

S. Roo.
34' Pipe

E

E

W 13

$\frac{5.4}{25}$ $\frac{5.9}{22}$ $\frac{6.4}{15}$ $\frac{7.2}{12}$ $\frac{6.7}{9}$ 6.6 $\frac{6.8}{5}$ $\frac{7.0}{7}$ $\frac{6.1}{9}$ $\frac{6.0}{25}$

$\frac{6.9}{25}$ $\frac{8.1}{14}$ $\frac{9.3}{10}$ $\frac{8.3}{8}$ 8.0 $\frac{8.3}{8}$ $\frac{8.8}{10}$ $\frac{7.9}{13}$ $\frac{7.9}{25}$

$\frac{8.4}{25}$ $\frac{9.4}{14}$ $\frac{10.2}{10}$ $\frac{9.9}{7}$ 9.6 $\frac{9.8}{8}$ $\frac{10.7}{9}$ $\frac{9.9}{11}$ $\frac{10.0}{25}$

$\frac{3.1}{25}$ $\frac{3.6}{16}$ $\frac{3.9}{10}$ $\frac{3.8}{8}$ 3.5 $\frac{3.8}{7}$ $\frac{4.6}{9}$ $\frac{3.9}{10}$ $\frac{4.8}{25}$

$\frac{4.4}{25}$ $\frac{4.5}{16}$ $\frac{5.0}{14}$ $\frac{4.2}{11}$ 4.2 $\frac{4.5}{6}$ $\frac{5.1}{8}$ $\frac{4.9}{10}$ $\frac{5.9}{25}$

$\frac{4.6}{25}$ $\frac{6.2}{16}$ $\frac{6.7}{F.L. 10}$ $\frac{4.6}{10}$ 4.8 $\frac{4.6}{4}$ $\frac{8.2}{F.L. 9}$ $\frac{8.5}{21}$ $\frac{8.8}{40}$

$\frac{4.3}{25}$ $\frac{4.7}{17}$ $\frac{4.5}{14}$ $\frac{5.4}{12}$ $\frac{4.1}{11}$ $\frac{4.6}{6}$ 4.6 $\frac{4.7}{4}$ $\frac{5.1}{6}$ $\frac{4.9}{8}$ $\frac{5.6}{25}$

$\frac{3.1}{25}$ $\frac{3.5}{13}$ $\frac{4.7}{10}$ $\frac{4.4}{9}$ $\frac{4.3}{5}$ 4.3 $\frac{4.6}{6}$ $\frac{4.1}{9}$ $\frac{3.6}{25}$

$\frac{1.8}{25}$ $\frac{2.1}{20}$ $\frac{3.0}{10}$ 3.1 $\frac{3.1}{7}$ $\frac{2.5}{16}$ $\frac{2.6}{25}$ $\frac{1.2}{50}$ $\frac{0.1}{65}$ $\frac{+0.5}{House}$

$\frac{2.2}{25}$ $\frac{2.7}{22}$ $\frac{2.5}{17}$ $\frac{3.5}{11}$ $\frac{4.8}{9}$ 4.5 $\frac{4.4}{5}$ $\frac{4.8}{7}$ $\frac{3.8}{9}$ $\frac{3.7}{25}$

57+0 + H.P. 121970. Elev. Remy
 78+0
 T.P. 2.37 1213.58 8.49 1211.21

79+0

80+0

81+0

82+0

83+0

83+73 = ϕ of culvert

R.M. & T.P. 6.29 121528 4.59 1208.99

84+0

85+0

86+0

X-07 S.M.
 Corner E.
 H.P. Elevation
 83+73

E. ϕ W. 14

$\frac{5.9}{25}$ $\frac{6.9}{17}$ $\frac{7.5}{10}$ $\frac{8.7}{8}$ $\frac{8.1}{7}$ 7.4 $\frac{7.8}{7}$ $\frac{8.2}{9}$ $\frac{7.2}{12}$ $\frac{7.2}{25}$

$\frac{3.8}{25}$ $\frac{4.0}{17}$ $\frac{3.5}{11}$ $\frac{4.2}{9}$ $\frac{3.1}{8}$ 2.9 $\frac{3.2}{8}$ $\frac{4.3}{16}$ $\frac{3.7}{12}$ $\frac{4.3}{17}$ $\frac{4.5}{25}$

$\frac{3.3}{25}$ $\frac{3.2}{20}$ $\frac{4.2}{12}$ $\frac{5.2}{9}$ $\frac{4.1}{7}$ 3.5 $\frac{4.1}{9}$ $\frac{5.0}{11}$ $\frac{3.7}{12}$ $\frac{4.1}{25}$

$\frac{4.8}{25}$ $\frac{5.4}{14}$ $\frac{6.3}{10}$ $\frac{5.7}{7}$ 5.0 $\frac{5.6}{8}$ $\frac{6.3}{11}$ $\frac{5.5}{15}$ $\frac{4.8}{25}$

$\frac{6.3}{25}$ $\frac{6.7}{15}$ $\frac{7.2}{10}$ $\frac{6.7}{8}$ 6.2 $\frac{6.6}{7}$ $\frac{7.5}{10}$ $\frac{6.9}{12}$ $\frac{6.2}{15}$ $\frac{6.3}{25}$

$\frac{7.7}{25}$ $\frac{7.4}{12}$ $\frac{7.6}{11}$ 6.9 $\frac{7.1}{7}$ $\frac{8.0}{10}$ $\frac{7.8}{12}$ $\frac{7.5}{14}$ $\frac{7.1}{25}$

$\frac{9.6}{30}$ $\frac{10.6}{12}$ $\frac{4.6}{9}$ $\frac{6.6}{9}$ 5.8 $\frac{5.1}{7}$ $\frac{4.8}{7}$ $\frac{10.1}{10}$ $\frac{10.1}{45}$ $\frac{10.1}{50}$

$\frac{9.3}{25}$ $\frac{9.5}{15}$ $\frac{7.7}{10}$ 7.9 $\frac{7.9}{5}$ $\frac{8.9}{7}$ $\frac{8.5}{9}$ $\frac{9.5}{25}$

$\frac{8.3}{25}$ $\frac{7.8}{16}$ $\frac{7.5}{13}$ $\frac{7.8}{11}$ $\frac{7.4}{9}$ $\frac{7.0}{2}$ 7.0 $\frac{7.5}{7}$ $\frac{7.4}{12}$ $\frac{7.5}{25}$

$\frac{4.8}{25}$ $\frac{5.1}{20}$ $\frac{5.7}{13}$ $\frac{6.4}{10}$ $\frac{5.8}{9}$ $\frac{5.6}{4}$ 5.7 $\frac{5.8}{3}$ $\frac{6.1}{6}$ $\frac{5.6}{9}$ $\frac{5.8}{25}$

Sta + H.I. F.O.V. Rod
 86+61 1215.28
 E of Drive on E. side of rd.

87+0

88+0

T.P. 11.33 1226.55 0.06 1215.22

89+0

89+22.2 E of E.S.W. Road

90+0

T.P. 7.82 1233.43 0.94 1225.61

91+0

92+0

93+0

94+0

B.M. 6.20 1227.23

North NE
 Root 4 rods
 Sta 93+70

E. W. 15

$\frac{5.3}{50}$ $\frac{4.4}{25}$ $\frac{4.7}{13}$ $\frac{5.2}{10}$ $\frac{4.8}{8}$ $\frac{4.3}{3}$ 4.5

$\frac{2.2}{25}$ $\frac{2.8}{15}$ $\frac{3.3}{13}$ $\frac{4.5}{10}$ $\frac{4.1}{9}$ $\frac{3.5}{3}$ 3.6 $\frac{3.8}{5}$ $\frac{4.5}{7}$ $\frac{3.0}{10}$ $\frac{2.9}{17}$ $\frac{2.5}{25}$

$\frac{7.0}{25}$ 0.4 $\frac{0.9}{11}$ $\frac{2.0}{8}$ $\frac{1.5}{7}$ $\frac{1.0}{2}$ 1.1 $\frac{1.5}{4}$ 2.2 $\frac{0.7}{10}$ $\frac{0.6}{17}$ $\frac{0.2}{25}$

$\frac{8.4}{25}$ $\frac{10.0}{20}$ $\frac{9.1}{15}$ $\frac{9.3}{8}$ 9.5 $\frac{9.2}{4}$ $\frac{8.8}{13}$ $\frac{1.8}{2.4}$ $\frac{7.2}{30}$

$\frac{6.2}{25}$ $\frac{8.1}{21}$ $\frac{7.8}{10}$ 8.3 $\frac{7.4}{6}$ $\frac{7.1}{18}$ $\frac{6.9}{25}$

$\frac{4.4}{25}$ $\frac{4.3}{19}$ $\frac{4.1}{13}$ $\frac{5.9}{8}$ $\frac{5.5}{4}$ 5.6 $\frac{5.5}{3}$ $\frac{5.8}{4}$ $\frac{5.0}{6}$ $\frac{3.9}{18}$ $\frac{3.5}{25}$

$\frac{7.6}{25}$ $\frac{7.2}{19}$ $\frac{7.0}{13}$ $\frac{9.3}{10}$ $\frac{9.0}{4}$ 9.1 $\frac{9.2}{2}$ $\frac{9.7}{3}$ $\frac{8.6}{5}$ $\frac{7.6}{14}$ $\frac{6.9}{25}$

$\frac{4.5}{25}$ $\frac{4.3}{19}$ $\frac{4.9}{12}$ $\frac{5.9}{10}$ $\frac{5.3}{4}$ 5.4 $\frac{5.5}{3}$ $\frac{5.8}{4}$ $\frac{5.1}{6}$ $\frac{4.6}{18}$ $\frac{4.5}{25}$

$\frac{4.0}{25}$ $\frac{4.1}{19}$ $\frac{4.6}{13}$ $\frac{5.6}{11}$ $\frac{5.1}{9}$ $\frac{4.7}{3}$ 4.8 $\frac{5.1}{5}$ $\frac{4.7}{7}$ $\frac{4.4}{25}$

$\frac{6.7}{25}$ $\frac{7.5}{14}$ $\frac{9.3}{8}$ $\frac{10.1}{6}$ $\frac{9.8}{3}$ 9.5 $\frac{9.5}{2}$ $\frac{10.3}{8}$ $\frac{9.3}{12}$ $\frac{9.4}{22}$ $\frac{9.6}{25}$

Sta + H.I. 1233 43

95+0

T.P. 3.615 1224.760 12.285 1221.145

96+0

97+0 House on W. side of rd.

97+33± E of Drive on W. side

98+0

98+10± E of Drive on W. side

98+70

99+0

T.P. 0.91 1213.35 12.32 1212.44

99+45

100+0

E.

E

W 16

$\frac{13.1}{25}$ $\frac{13.2}{21}$ $\frac{13.4}{11}$ $\frac{13.4}{5}$ $\frac{12.2}{2}$ 12.1 $\frac{12.1}{7}$ $\frac{12.4}{11}$ $\frac{12.7}{13}$ $\frac{12.8}{25}$

$\frac{4.9}{25}$ $\frac{5.0}{19}$ $\frac{4.9}{14}$ $\frac{4.6}{5}$ $\frac{4.8}{2}$ 4.6 $\frac{4.2}{7}$ $\frac{4.6}{11}$ $\frac{4.9}{12}$ $\frac{4.5}{16}$ $\frac{4.0}{25}$

$\frac{5.9}{25}$ $\frac{5.7}{10}$ $\frac{5.4}{4}$ $\frac{5.2}{2}$ 5.1 $\frac{5.0}{7}$ $\frac{4.8}{12}$ $\frac{4.2}{25}$ $\frac{1.4}{House}$

5.2 $\frac{5.1}{12}$ $\frac{4.5}{17}$ $\frac{3.9}{25}$

$\frac{5.9}{25}$ $\frac{6.0}{15}$ $\frac{6.0}{5}$ $\frac{7.6}{2}$ 7.9 $\frac{7.6}{7}$ $\frac{7.7}{13}$ $\frac{7.3}{18}$ $\frac{7.6}{25}$

8.5 $\frac{8.1}{7}$ $\frac{8.1}{6}$ $\frac{8.1}{12}$ $\frac{8.4}{13}$ $\frac{7.5}{15}$ $\frac{8.0}{25}$

$\frac{9.1}{25}$ $\frac{8.8}{14}$ $\frac{8.5}{6}$ $\frac{9.7}{2}$ 9.5 $\frac{9.4}{5}$ $\frac{9.6}{11}$ $\frac{8.5}{13}$ $\frac{8.4}{25}$

$\frac{10.8}{25}$ $\frac{10.6}{16}$ $\frac{10.8}{5}$ $\frac{11.7}{2}$ 11.6 $\frac{11.6}{5}$ $\frac{11.6}{11}$ $\frac{10.3}{15}$ $\frac{9.7}{19}$ $\frac{9.4}{25}$

$\frac{2.5}{25}$ $\frac{2.9}{16}$ $\frac{3.7}{6}$ $\frac{4.2}{3}$ $\frac{3.8}{2}$ 3.8 $\frac{3.7}{3}$ $\frac{3.9}{8}$ $\frac{4.5}{10}$ $\frac{3.6}{12}$ $\frac{3.0}{17}$ $\frac{2.8}{25}$

$\frac{5.5}{25}$ $\frac{5.5}{15}$ $\frac{5.5}{6}$ $\frac{6.1}{5}$ $\frac{5.2}{3}$ 5.4 $\frac{5.2}{2}$ $\frac{5.5}{7}$ $\frac{6.1}{7}$ $\frac{5.7}{10}$ $\frac{5.6}{24}$ $\frac{5.8}{25}$

Sta + H. I. - Elev Rems. - E

1213 35

v. 17

101+0

$\frac{8.3}{25}$ $\frac{7.6}{15}$ $\frac{7.9}{7}$ $\frac{8.1}{6}$ $\frac{7.5}{4}$ 7.2 $\frac{7.1}{2}$ $\frac{7.4}{7}$ $\frac{8.2}{10}$ $\frac{7.9}{16}$ $\frac{8.1}{25}$

102+0

$\frac{8.3}{25}$ $\frac{8.5}{16}$ $\frac{8.5}{12}$ $\frac{9.1}{9}$ $\frac{9.5}{7}$ $\frac{9.0}{6}$ 8.5 $\frac{8.7}{4}$ $\frac{9.3}{7}$ $\frac{9.9}{9}$ $\frac{8.5}{11}$ $\frac{8.7}{18}$ $\frac{8.9}{25}$

T.P. 2.775 1206.905 9.22 1204.13

103+0

$\frac{2.8}{25}$ $\frac{2.4}{18}$ $\frac{3.5}{8}$ $\frac{4.0}{6}$ $\frac{3.7}{5}$ 3.2 $\frac{3.5}{8}$ $\frac{4.5}{9}$ $\frac{3.7}{11}$ $\frac{3.5}{19}$ $\frac{3.2}{25}$

104+0

$\frac{5.2}{25}$ $\frac{4.6}{9}$ $\frac{4.3}{4}$ $\frac{4.9}{3}$ $\frac{4.2}{2}$ 4.3 $\frac{4.0}{4}$ $\frac{4.2}{11}$ $\frac{5.2}{13}$ $\frac{4.6}{14}$ $\frac{4.9}{20}$ $\frac{5.4}{25}$

104+72.5 ± of Culvert

$\frac{6.7}{16}$ $\frac{2.3}{7}$ $\frac{3.7}{7}$ 3.7 $\frac{3.6}{10}$ $\frac{2.2}{10}$ $\frac{6.8}{12}$ $\frac{6.8}{17}$

B.M. 2.16 1204.745 x on

105+0

$\frac{5.6}{25}$ $\frac{5.5}{16}$ $\frac{5.0}{6}$ $\frac{4.7}{3}$ 4.8 $\frac{4.6}{8}$ $\frac{4.7}{11}$ $\frac{5.3}{12}$ $\frac{5.1}{15}$ $\frac{5.2}{20}$ $\frac{5.2}{25}$

106+0

$\frac{5.1}{25}$ $\frac{5.4}{17}$ $\frac{4.4}{6}$ $\frac{5.1}{5}$ $\frac{4.4}{3}$ 4.3 $\frac{4.2}{7}$ $\frac{4.9}{9}$ $\frac{4.6}{10}$ $\frac{4.9}{19}$ $\frac{5.1}{25}$

107+0

$\frac{4.9}{25}$ $\frac{4.8}{19}$ $\frac{4.1}{9}$ $\frac{4.5}{7}$ $\frac{3.9}{6}$ 3.8 $\frac{3.8}{5}$ $\frac{4.2}{6}$ $\frac{4.0}{8}$ $\frac{4.5}{15}$ $\frac{4.6}{25}$

June 11, 1927

Sta + H.I. -

B.M. 2.975 1207.720

108+0

108+11 1203.6

109+0

T.P. 4.76 1210.59 1.89 1205.83

110+0

111+0

111+48 \pm of 4" Drain Tile

112+0

T.P. 6.75 1215.85 1.49 1209.10

113+0

114+0

T.P. 8.65 1223.66 0.84 1215.01

1204745 1 on 8 in.
Copper
2 1/2 in.
3 1/2 in.
4 1/2 in.
5 1/2 in.
6 1/2 in.
7 1/2 in.
8 1/2 in.
9 1/2 in.
10 1/2 in.
11 1/2 in.
12 1/2 in.

E.

C

18

$\frac{2.2}{25}$ $\frac{3.6}{20}$ $\frac{4.2}{12}$ $\frac{4.8}{10}$ $\frac{4.4}{8}$ $\frac{4.2}{3}$ 4.3 $\frac{4.4}{5}$ $\frac{3.3}{7}$ $\frac{4.0}{12}$ $\frac{3.5}{25}$

$\frac{0.9}{27}$ $\frac{3.2}{22}$ $\frac{3.8}{12}$ $\frac{4.9}{9}$ $\frac{4.3}{7}$ $\frac{4.0}{3}$ 4.1 $\frac{4.2}{2}$ $\frac{4.3}{5}$ $\frac{3.3}{8}$ $\frac{2.8}{19}$ $\frac{3.1}{25}$

$\frac{0.4}{25}$ $\frac{3.3}{19}$ $\frac{3.0}{9}$ $\frac{2.1}{3}$ 2.5 $\frac{2.6}{2}$ $\frac{3.2}{6}$ $\frac{2.0}{9}$ $\frac{0.7}{19}$ $\frac{1.8}{25}$

$\frac{5.7}{25}$ $\frac{5.2}{10}$ $\frac{4.9}{7}$ 4.1 $\frac{4.3}{5}$ $\frac{4.8}{6}$ $\frac{4.4}{8}$ $\frac{4.9}{18}$ $\frac{5.3}{25}$

$\frac{5.0}{25}$ $\frac{4.8}{14}$ $\frac{4.1}{3}$ 3.6 $\frac{3.3}{4}$ $\frac{3.7}{8}$ $\frac{3.4}{10}$ $\frac{3.8}{18}$ $\frac{4.7}{25}$

$\frac{5.4}{25}$ $\frac{3.6}{10}$ 3.2 $\frac{2.9}{5}$ $\frac{3.3}{10}$ $\frac{2.9}{12}$ $\frac{3.8}{14}$ $\frac{4.2}{25}$

$\frac{4.8}{25}$ $\frac{3.4}{10}$ $\frac{2.4}{3}$ $\frac{3.0}{7}$ 2.5 $\frac{2.1}{5}$ $\frac{2.7}{17}$ $\frac{2.3}{13}$ $\frac{3.1}{19}$ $\frac{2.8}{25}$

$\frac{7.0}{25}$ $\frac{6.3}{11}$ $\frac{6.3}{5}$ $\frac{6.7}{2}$ 6.3 $\frac{5.8}{5}$ $\frac{6.8}{12}$ $\frac{5.9}{14}$ $\frac{5.3}{18}$ $\frac{5.5}{25}$

$\frac{3.6}{25}$ $\frac{0.7}{5}$ $\frac{4.8}{2}$ 4.5 $\frac{4.2}{2}$ $\frac{5.2}{10}$ $\frac{3.7}{14}$ $\frac{3.8}{25}$

5th + H. 1223.22 Fish Reels

115+0

116+0

117+0

T.P. 5.96 1226.26 3.36 1220.30

118+0

119+0

120+0

T.P. 5.56 1229.745 2.075 1224.185

121+0

122+0

123+0

T.P. 6.025 1235.12 0.65 1229.095

13.M 1.59 1233.53

F E 19

$\frac{5.4}{25}$ $\frac{6.1}{11}$ $\frac{9.9}{4}$ 9.1 $\frac{9.4}{8}$ $\frac{10.3}{10}$ $\frac{6.9}{15}$ $\frac{.4}{25}$

$\frac{3.4}{25}$ $\frac{3.2}{17}$ $\frac{4.4}{8}$ $\frac{6.5}{5}$ 5.4 $\frac{5.3}{3}$ $\frac{5.8}{7}$ $\frac{6.8}{10}$ $\frac{4.2}{14}$ $\frac{4.2}{25}$

$\frac{2.5}{25}$ $\frac{2.4}{15}$ $\frac{3.0}{6}$ $\frac{4.0}{3}$ 3.2 $\frac{3.2}{5}$ $\frac{3.5}{8}$ $\frac{4.4}{11}$ $\frac{2.9}{14}$ $\frac{2.5}{25}$

$\frac{4.8}{25}$ $\frac{4.7}{13}$ $\frac{4.6}{1}$ 5.5 $\frac{4.8}{1}$ $\frac{4.6}{6}$ $\frac{5.1}{11}$ $\frac{5.7}{12}$ $\frac{4.2}{15}$ $\frac{4.8}{25}$

$\frac{4.2}{25}$ $\frac{4.3}{15}$ $\frac{4.2}{5}$ 4.0 $\frac{3.5}{5}$ $\frac{4.4}{13}$ $\frac{3.7}{15}$ $\frac{4.1}{25}$

$\frac{2.8}{25}$ $\frac{2.9}{15}$ $\frac{2.8}{5}$ 2.6 $\frac{2.6}{5}$ $\frac{3.0}{13}$ $\frac{3.5}{25}$

$\frac{5.7}{25}$ $\frac{5.4}{12}$ $\frac{5.1}{4}$ 4.8 $\frac{4.8}{2}$ $\frac{5.6}{7}$ $\frac{4.8}{11}$ $\frac{5.2}{15}$ $\frac{5.5}{25}$

$\frac{3.7}{25}$ $\frac{3.6}{9}$ $\frac{4.0}{6}$ 3.2 $\frac{4.2}{6}$ $\frac{3.7}{9}$ $\frac{3.4}{14}$ $\frac{3.3}{25}$

$\frac{1.8}{25}$ $\frac{1.5}{11}$ $\frac{2.6}{7}$ 1.8 $\frac{2.2}{5}$ $\frac{2.7}{7}$ $\frac{1.8}{9}$ $\frac{1.3}{11}$ $\frac{0.7}{25}$

Sta + H.I. - Elev. Rem's

E. E. W. 20

B.M. 1.45 123478 123353

124+0

$\frac{4.2}{25}$ $\frac{4.0}{22}$ $\frac{4.9}{9}$ $\frac{5.5}{4}$ 5.1 $\frac{5.9}{6}$ $\frac{4.1}{11}$ $\frac{4.2}{17}$ $\frac{3.8}{25}$

125+0

$\frac{1.2}{40}$ $\frac{1.5}{25}$ $\frac{1.4}{23}$ $\frac{2.2}{10}$ $\frac{2.8}{5}$ 2.6 $\frac{2.5}{8}$ $\frac{3.1}{11}$ $\frac{1.3}{15}$ $\frac{0.8}{25}$

T.P. 8.78 124296 080 123412

125+41 $\frac{1}{2}$ of W. Road

$\frac{7.5}{25}$ $\frac{7.6}{19}$ $\frac{7.8}{11}$ $\frac{8.8}{7}$ 8.7 $\frac{7.9}{10}$ $\frac{6.5}{13}$ $\frac{6.8}{30}$

126+0

$\frac{6.2}{25}$ $\frac{6.0}{13}$ $\frac{6.7}{8}$ 6.4 $\frac{6.0}{10}$ $\frac{6.5}{13}$ $\frac{5.7}{16}$ $\frac{5.2}{25}$

127+0

$\frac{2.7}{25}$ $\frac{3.3}{11}$ $\frac{4.3}{8}$ 3.9 $\frac{4.1}{7}$ $\frac{4.4}{10}$ $\frac{2.6}{13}$ $\frac{1.8}{19}$ $\frac{1.6}{25}$

T.P. 6.52 1246.89 2.59 1240.37

128+0

$\frac{5.9}{25}$ $\frac{5.7}{17}$ $\frac{6.1}{11}$ $\frac{6.1}{7}$ 5.6 $\frac{6.0}{5}$ $\frac{6.5}{8}$ $\frac{5.5}{10}$ $\frac{5.6}{19}$ $\frac{5.4}{25}$

129+0

$\frac{4.5}{25}$ $\frac{4.9}{18}$ $\frac{5.4}{7}$ 4.8 $\frac{5.3}{9}$ $\frac{5.4}{15}$ $\frac{4.4}{25}$

130+0

$\frac{3.9}{25}$ $\frac{4.0}{16}$ $\frac{4.7}{7}$ 4.1 $\frac{4.7}{6}$ $\frac{4.2}{12}$ $\frac{4.4}{25}$

T.P. 0.71 1243.07 4.53 124236

131+0

$\frac{0.3}{25}$ $\frac{0.4}{16}$ $\frac{1.1}{8}$ 0.4 $\frac{0.9}{5}$ $\frac{0.4}{13}$ $\frac{0.6}{25}$

132+0

$\frac{1.5}{25}$ $\frac{1.8}{12}$ $\frac{2.3}{8}$ $\frac{1.9}{3}$ 2.2 $\frac{2.6}{4}$ $\frac{1.9}{8}$ $\frac{2.0}{20}$ $\frac{2.1}{25}$

B.M. 3.02 124005

W.
Nail in
Notch s.
16" angle

Sta + H.I. - Elev. Rems
 B.M. 2.92 1242.77 1240.05 Nail in
 Notes
 S. Root
 132+
 N. 1000

133+0

134+0

135+0
 T.P. 3.98 1239.32 7.63 1235.34

136+0

137+0

137+91 ± of Culvert (10° C.I.P.)

138+0

139+0 on the Arc

T.P. 10.35 1246.08 3.59 1235.73

140

141+0

E. June 13. 929 Fog
 Gold J. 2
 S. Merritt
 H. Barton W

$\frac{2.2}{25}$ $\frac{2.7}{17}$ $\frac{3.6}{10}$ $\frac{4.8}{7}$ 4.2 $\frac{4.6}{7}$ $\frac{3.5}{11}$ $\frac{3.2}{21}$ $\frac{3.1}{25}$

$\frac{4.7}{25}$ $\frac{4.8}{19}$ $\frac{5.8}{10}$ $\frac{6.5}{6}$ 6.0 $\frac{6.5}{9}$ $\frac{5.8}{12}$ $\frac{5.6}{20}$ $\frac{5.5}{25}$

$\frac{7.7}{25}$ $\frac{7.9}{15}$ $\frac{7.4}{4}$ 7.4 $\frac{7.6}{8}$ $\frac{9.0}{23}$ $\frac{9.1}{25}$

$\frac{3.9}{25}$ $\frac{4.6}{8}$ 4.8 $\frac{4.2}{9}$ $\frac{4.5}{15}$ $\frac{4.3}{25}$

$\frac{4.5}{25}$ $\frac{4.5}{18}$ $\frac{4.4}{9}$ 5.1 $\frac{4.8}{3}$ $\frac{4.9}{4}$ $\frac{4.7}{5}$ $\frac{4.5}{12}$ $\frac{5.0}{18}$ $\frac{5.1}{25}$

$\frac{4.1}{25}$ $\frac{4.3}{17}$ $\frac{4.6}{9}$ 5.2 $\frac{5.3}{FL.}$ $\frac{4.5}{7}$ $\frac{4.5}{13}$ $\frac{4.7}{18}$ $\frac{5.4}{FL.}$ $\frac{5.9}{25}$

$\frac{3.9}{25}$ $\frac{4.2}{18}$ $\frac{4.7}{7}$ 5.2 $\frac{5.2}{4}$ $\frac{4.7}{6}$ $\frac{5.0}{7}$ $\frac{4.7}{9}$ $\frac{4.6}{14}$ $\frac{4.6}{20}$ $\frac{5.3}{25}$

$\frac{4.0}{25}$ $\frac{3.7}{16}$ $\frac{3.8}{7}$ 4.2 $\frac{3.9}{8}$ $\frac{4.2}{16}$ $\frac{4.3}{25}$

S. $\frac{8.6}{25}$ $\frac{8.4}{21}$ $\frac{8.7}{11}$ $\frac{8.9}{5}$ 10.1 $\frac{9.5}{7}$ $\frac{10.1}{14}$ $\frac{9.1}{16}$ $\frac{8.8}{25}$

N. $\frac{7.1}{25}$ $\frac{6.7}{14}$ $\frac{7.1}{4}$ 8.5 $\frac{8.0}{6}$ $\frac{8.5}{13}$ $\frac{6.9}{15}$ $\frac{7.0}{17}$ $\frac{6.5}{25}$

Sta	+	H. I	-	Elev.	Remarks
B.M.		1246.08		4.62	1241.46 Nail in SE Root 22' Maple Sta 141+98 S-21' El. 1241.46
142+0					

142+18± E of Drive N. Side

143+0 House on N. Side

143+17± E of Drive S. Side

144+0

145+0

T.P. 2.92 1239.66 9.34 1236.74

146+0

147+0

148+0

149+0

S. E. N. 22

$\frac{5.5}{25}$ $\frac{5.4}{10}$ $\frac{5.5}{3}$ 6.3 $\frac{5.7}{6}$ $\frac{6.2}{11}$ $\frac{4.8}{16}$ $\frac{5.1}{25}$

6.0 $\frac{5.5}{6}$ $\frac{5.8}{10}$ $\frac{5.1}{25}$ $\frac{4.9}{35}$

$\frac{3.8}{16}$ $\frac{4.8}{10}$ $\frac{4.9}{3}$ 5.6 $\frac{5.7}{5}$ $\frac{5.6}{11}$ $\frac{5.1}{18}$ $\frac{5.0}{25}$ $\frac{2.2}{House}$

$\frac{5.9}{39}$ $\frac{5.6}{20}$ $\frac{5.6}{8}$ 5.7

$\frac{6.3}{25}$ $\frac{6.3}{20}$ $\frac{6.5}{8}$ 6.4 $\frac{7.6}{3}$ $\frac{7.3}{10}$ $\frac{7.0}{15}$ $\frac{6.6}{20}$ $\frac{6.6}{25}$

$\frac{7.1}{25}$ $\frac{7.3}{12}$ 7.7 $\frac{9.4}{3}$ $\frac{8.8}{10}$ $\frac{9.2}{17}$ $\frac{8.6}{25}$

$\frac{2.9}{25}$ $\frac{2.9}{19}$ $\frac{3.1}{9}$ 3.1 $\frac{4.9}{3}$ $\frac{4.3}{11}$ $\frac{4.9}{20}$ $\frac{5.8}{25}$

$\frac{5.2}{25}$ $\frac{5.3}{20}$ $\frac{5.2}{8}$ $\frac{6.0}{2}$ 5.6 $\frac{7.2}{5}$ $\frac{6.5}{12}$ $\frac{7.1}{21}$ $\frac{5.7}{25}$

$\frac{7.4}{25}$ 8.2 $\frac{7.9}{1}$ $\frac{9.4}{6}$ $\frac{8.5}{12}$ $\frac{9.0}{18}$ $\frac{9.6}{21}$ $\frac{8.2}{25}$

$\frac{9.5}{25}$ $\frac{9.3}{16}$ $\frac{9.7}{1}$ 9.4 $\frac{11.3}{5}$ $\frac{10.6}{13}$ $\frac{11.6}{20}$ $\frac{11.0}{25}$

Sta + H.V. Elev. Cont.
1239.6
T.P. 1.20 1229.13 11.73 1227.93

150+0

151+0

B.M. Established

3.37

1225.76 151+19

152+0

153+0

154+0

155+0

T.P. 7.64 1230.14 6.63 1222.50

155+08± 4" Tile

156+0

157+0

158+0

5. 4 N 23

$\frac{1.0}{25}$ $\frac{1.2}{11}$ $\frac{2.1}{2}$ 1.3 $\frac{2.4}{3}$ $\frac{2.6}{5}$ $\frac{2.1}{12}$ $\frac{3.9}{19}$ $\frac{2.3}{25}$

$\frac{3.4}{25}$ $\frac{3.5}{15}$ $\frac{3.8}{3}$ $\frac{4.3}{2}$ $\frac{4.2}{2}$ 3.8 $\frac{3.8}{2}$ $\frac{4.0}{4}$ $\frac{3.9}{10}$ $\frac{4.1}{17}$ $\frac{3.7}{25}$

$\frac{6.0}{25}$ $\frac{6.8}{7}$ $\frac{6.1}{8}$ $\frac{5.4}{3}$ $\frac{5.9}{2}$ 5.3 $\frac{5.2}{2}$ $\frac{5.0}{8}$ $\frac{5.1}{14}$ $\frac{5.5}{25}$

$\frac{7.7}{25}$ $\frac{7.5}{11}$ $\frac{7.1}{2}$ 6.7 $\frac{6.3}{2}$ $\frac{5.7}{7}$ $\frac{6.0}{14}$ $\frac{6.9}{20}$ $\frac{6.9}{25}$

$\frac{6.6}{25}$ $\frac{8.3}{10}$ 7.9 $\frac{6.8}{4}$ $\frac{6.4}{5}$ $\frac{6.8}{15}$ $\frac{7.7}{21}$ $\frac{7.8}{25}$

$\frac{8.2}{25}$ $\frac{8.1}{14}$ $\frac{7.9}{5}$ 7.6 $\frac{7.1}{4}$ $\frac{6.6}{10}$ $\frac{7.4}{17}$ $\frac{7.4}{25}$

$\frac{9.3}{25}$ $\frac{8.9}{10}$ 8.4 $\frac{8.1}{4}$ $\frac{7.6}{11}$ $\frac{8.2}{16}$ $\frac{8.5}{18}$ $\frac{8.0}{19}$ $\frac{8.3}{25}$ $\frac{10.1}{27}$ $\frac{10.5}{25}$

$\frac{9.4}{25}$ $\frac{9.2}{21}$ $\frac{8.8}{8}$ 8.6 $\frac{7.7}{10}$ $\frac{7.9}{16}$ $\frac{8.4}{17}$ $\frac{7.9}{19}$ $\frac{8.4}{25}$

$\frac{7.0}{25}$ $\frac{6.9}{18}$ $\frac{7.5}{5}$ $\frac{7.3}{3}$ 7.5 $\frac{7.9}{4}$ $\frac{7.3}{11}$ $\frac{7.6}{18}$ $\frac{7.6}{25}$

$\frac{4.9}{25}$ $\frac{5.0}{11}$ $\frac{5.1}{7}$ $\frac{5.0}{1}$ 6.1 $\frac{6.8}{2}$ $\frac{6.4}{11}$ $\frac{7.0}{19}$ $\frac{5.7}{25}$

3+6 + H. 1230. 14

E/CV Ret 23

159+0

160+0

160+7± E of Drive N. side of Rd.

161+0

162+0

T.P. 3.29 1231.17 2.26 1227.88

163+0

B.M. 1.98 1229.19

164+0

Nail in
5' Root
16' Mark
N side
163+01

165+0

165+4± E of Drive S. Side of Rd.

166+0

5. E N. 24

$\frac{3.8}{25} \frac{4.4}{6} \frac{4.2}{4} 5.5 \frac{5.2}{9} \frac{5.9}{17} \frac{4.5}{2} \frac{4.0}{25}$

$\frac{2.4}{25} \frac{2.4}{16} \frac{2.3}{8} \frac{3.4}{3} \frac{3.7}{2} 3.5 \frac{3.3}{5} \frac{3.8}{12} \frac{2.1}{16} \frac{1.8}{25}$

$2.3 \frac{2.2}{5} \frac{2.4}{7} \frac{2.1}{16} \frac{1.4}{25} \frac{0.7}{House}$

$\frac{1.9}{25} \frac{1.9}{18} \frac{2.1}{9} \frac{2.8}{5} 2.2 \frac{2.0}{4} \frac{2.4}{11} \frac{1.4}{14} \frac{1.6}{25}$

$\frac{1.7}{25} \frac{1.7}{18} \frac{2.0}{8} \frac{2.4}{2} 1.9 \frac{1.8}{6} \frac{2.5}{14} \frac{1.8}{18} \frac{1.6}{25}$

$\frac{3.7}{25} \frac{3.7}{19} \frac{4.0}{8} \frac{3.9}{4} \frac{4.3}{1} 4.1 \frac{3.7}{7} \frac{4.3}{15} \frac{3.4}{20} \frac{2.8}{25}$

$\frac{4.4}{25} \frac{4.9}{10} \frac{5.2}{4} 4.7 \frac{4.4}{4} \frac{5.3}{11} \frac{4.9}{13} \frac{5.3}{18} \frac{5.9}{25}$

$\frac{3.6}{25} \frac{3.8}{18} \frac{4.6}{11} \frac{5.8}{6} 5.9 \frac{6.2}{8} \frac{4.8}{11} \frac{6.2}{13} \frac{5.2}{16} \frac{3.3}{25}$

$\frac{4.8}{25} \frac{4.9}{23} \frac{5.2}{14} \frac{6.0}{6} 6.5$

$\frac{4.5}{House} \frac{5.0}{25} \frac{5.4}{21} \frac{5.3}{13} \frac{6.2}{9} \frac{7.8}{6} 8.5 \frac{8.4}{4} \frac{8.6}{9} \frac{9.0}{11} \frac{7.5}{14} \frac{6.3}{19} \frac{6.3}{25}$

Sta + 1231 17
166+50
T.P. 3.61 1224.02 10.76 1220.41

167+0

168+0
T.P. 0.47 1213.29 11.20 1212.82

169+0

170+0

171+0
T.P. 2.49 1207.29 8.49 1204.80

172+0

173+0

174+0

B.M.

175+0

5.66 1201.63 Nail in N.
Root
20" Maple
24" S
Sta 174+01
El. 1201.63

5 E N. 25
 $\frac{6.3}{25}$ $\frac{6.0}{17}$ $\frac{7.2}{9}$ $\frac{10.8}{4}$ 10.7 $\frac{10.6}{5}$ $\frac{11.5}{12}$ $\frac{9.0}{15}$ $\frac{8.2}{19}$ $\frac{8.2}{25}$

$\frac{0.4}{25}$ $\frac{0.5}{20}$ $\frac{1.4}{10}$ $\frac{6.3}{3}$ 5.9 $\frac{5.8}{9}$ $\frac{6.7}{12}$ $\frac{3.5}{17}$ $\frac{2.9}{25}$

$\frac{6.2}{25}$ $\frac{5.8}{11}$ $\frac{11.3}{2}$ 10.9 $\frac{10.5}{5}$ $\frac{10.7}{9}$ $\frac{11.2}{11}$ $\frac{9.3}{15}$ $\frac{8.2}{20}$ $\frac{7.4}{25}$

$\frac{3.3}{25}$ $\frac{3.1}{19}$ $\frac{3.0}{7}$ $\frac{3.8}{4}$ 3.5 $\frac{3.1}{3}$ $\frac{3.7}{11}$ $\frac{3.3}{18}$ $\frac{2.4}{25}$

$\frac{6.3}{25}$ $\frac{5.9}{21}$ $\frac{5.8}{13}$ $\frac{6.0}{7}$ 5.5 $\frac{6.4}{5}$ $\frac{5.6}{8}$ $\frac{5.8}{16}$ $\frac{5.8}{25}$

$\frac{8.3}{25}$ $\frac{8.1}{18}$ $\frac{7.8}{12}$ $\frac{6.9}{10}$ $\frac{8.2}{9}$ $\frac{7.9}{7}$ 7.6 $\frac{8.2}{4}$ $\frac{8.0}{10}$ $\frac{7.9}{14}$ $\frac{8.1}{25}$

$\frac{3.4}{25}$ $\frac{3.7}{18}$ $\frac{2.9}{10}$ $\frac{3.8}{8}$ $\frac{3.4}{7}$ $\frac{3.1}{2}$ 3.1 $\frac{3.3}{5}$ $\frac{3.4}{12}$ $\frac{3.3}{16}$ $\frac{3.1}{25}$

$\frac{5.2}{25}$ $\frac{5.0}{19}$ $\frac{4.8}{10}$ $\frac{5.5}{8}$ $\frac{4.8}{7}$ 4.5 $\frac{4.5}{7}$ $\frac{4.9}{14}$ $\frac{4.3}{21}$ $\frac{4.3}{25}$

$\frac{6.7}{25}$ $\frac{6.1}{19}$ $\frac{5.8}{11}$ $\frac{6.1}{9}$ $\frac{6.9}{7}$ $\frac{6.3}{6}$ 6.0 $\frac{6.7}{4}$ $\frac{6.5}{7}$ $\frac{6.0}{12}$ $\frac{6.2}{25}$

$\frac{8.1}{25}$ $\frac{7.5}{20}$ $\frac{6.9}{14}$ $\frac{8.6}{7}$ 7.6 $\frac{7.7}{3}$ $\frac{8.6}{7}$ $\frac{6.9}{13}$ $\frac{6.0}{15}$ $\frac{5.4}{25}$

Sta + H.I. - Elev. Rms

B.M. 4.71 1206.34 1201.63 *naulin*

175+45

T.P. 1.595 1198.88 9.055 1197.285

176+0

176+57

177+0

178+0

178+10± E of CULVERT

T.P. 6.37 1198.27 6.98 1191.90

179+0

180+0

T.P. 11.02 1207.85 1.44 1196.83

181+0

$\frac{8.1}{7.5} \frac{7.6}{20} \frac{7.4}{13} \frac{9.3}{8} \frac{8.7}{6} 8.2 \frac{8.6}{2} \frac{9.5}{9} \frac{8.6}{11} \frac{5.7}{15} \frac{5.1}{25}$

$\frac{3.0}{25} \frac{2.6}{20} \frac{2.4}{13} \frac{5.0}{8} \frac{4.3}{2} 4.0 \frac{4.2}{6} \frac{5.0}{7} \frac{0.0}{18} \frac{+0.7}{25}$

$\frac{7.3}{25} \frac{6.7}{22} \frac{6.1}{14} \frac{7.0}{8} 6.8 \frac{7.0}{10} \frac{6.0}{12} \frac{2.6}{25}$

$\frac{9.9}{25} \frac{8.7}{15} \frac{8.1}{6} 8.0 \frac{7.9}{12} \frac{7.8}{19} \frac{8.2}{25}$

$\frac{10.1}{35} \frac{11.0}{15} \frac{11.4}{7} 8.6 \frac{8.4}{12} \frac{10.3}{15} \frac{10.8}{25}$

$\frac{10.2}{20} \frac{11.9}{12} \frac{13.4}{FL. 5} \frac{7.0}{2} \frac{8.5}{2} 8.5 \frac{8.3}{13} \frac{7.0}{13} \frac{13.1}{FL. 5} \frac{13.7}{23}$

$\frac{9.3}{25} \frac{9.4}{9} 9.0 \frac{7.9}{3} \frac{7.4}{9} \frac{7.6}{15} \frac{8.1}{17} \frac{9.7}{25}$

$\frac{0.6}{25} \frac{0.7}{22} \frac{0.7}{18} \frac{3.5}{12} \frac{4.4}{7} \frac{3.7}{5} 3.5 3.5 \frac{4.0}{2} \frac{3.5}{11} \frac{1.4}{17} \frac{0.5}{19} \frac{0.3}{23} \frac{0.3}{25}$

$\frac{5.4}{25} \frac{5.6}{22} \frac{5.9}{12} 8.8 \frac{7.8}{6} 8.7 \frac{8.1}{10} \frac{5.8}{16} \frac{5.5}{21} \frac{5.6}{25}$

Sta + Elev Rem's

182+0

120765

182+25+ \pm of Drive on S. Side of Rd.

183+0

T.P. 4.22 1207.085 4.985 1202865

B.M. 0.205 1206885

183+91+ \pm of 12" C.I.P.

Wall in
North
N W Root
24" Maple
5-27' dia
183+20
Fl. 1206885

184+0

T.P. 13.01 1215.865 4.23 1202.855

185+0

185+64

186+0

T.P. 7.06 1221.99 0.935 1214.930

186+90

187+0

5

N. 21

$$\begin{array}{cccccccc} +0.3 & 0.7 & 1.1 & 1.4 & 3.8 & 3.7 & 3.5 & 3.9 & 2.1 & 2.3 \\ \text{House} & \frac{25}{25} & \frac{17}{17} & \frac{9}{9} & \frac{4}{4} & & \frac{4}{4} & \frac{10}{10} & \frac{13}{13} & \frac{25}{25} \end{array}$$

$$\frac{1.3}{25} \quad \frac{1.7}{20} \quad \frac{2.5}{7} \quad 3.0 \quad \frac{3.0}{4} \quad \frac{3.7}{9} \quad \frac{1.9}{12} \quad \frac{1.6}{18} \quad \frac{2.0}{25}$$

$$\frac{1.4}{31} \quad \frac{3.3}{17} \quad \frac{4.2}{6} \quad \frac{5.7}{8} \quad 5.6 \quad \frac{5.3}{5} \quad \frac{6.1}{11} \quad \frac{7.0}{19} \quad \frac{7.7}{25}$$

$$\frac{7.2}{25} \quad \frac{7.6}{20} \quad \frac{7.6}{FL.} \quad \frac{4.9}{5} \quad 4.8 \quad \frac{4.7}{2} \quad \frac{5.0}{7} \quad \frac{7.1}{10} \quad \frac{8.3}{FL.} \quad \frac{8.0}{21} \quad \frac{8.0}{25} \quad \frac{8.4}{35}$$

$$\frac{7.2}{25} \quad \frac{7.5}{20} \quad \frac{7.0}{10} \quad \frac{5.1}{8} \quad \frac{4.8}{4} \quad 4.7 \quad \frac{4.6}{2} \quad \frac{5.0}{8} \quad \frac{7.2}{13} \quad \frac{8.0}{25}$$

$$\frac{13.2}{25} \quad \frac{13.0}{17} \quad \frac{12.6}{10} \quad \frac{11.7}{2} \quad 12.0 \quad \frac{12.3}{2} \quad \frac{12.6}{14} \quad \frac{12.6}{21} \quad \frac{12.8}{25}$$

$$\frac{8.0}{25} \quad \frac{7.8}{18} \quad \frac{10.5}{12} \quad \frac{9.6}{4} \quad 10.1 \quad \frac{10.7}{5} \quad \frac{6.5}{12} \quad \frac{5.9}{20} \quad \frac{6.0}{25}$$

$$\frac{4.4}{25} \quad \frac{4.2}{21} \quad \frac{8.2}{12} \quad \frac{7.8}{5} \quad 8.0 \quad \frac{8.2}{3} \quad \frac{4.0}{9} \quad \frac{3.4}{10} \quad \frac{3.1}{17} \quad \frac{3.3}{25}$$

$$\frac{5.6}{25} \quad \frac{5.3}{20} \quad \frac{5.2}{12} \quad \frac{7.0}{9} \quad \frac{6.0}{3} \quad 6.2 \quad \frac{6.6}{4} \quad \frac{5.9}{5} \quad \frac{4.8}{10} \quad \frac{5.1}{14} \quad \frac{6.3}{25}$$

$$\frac{4.9}{25} \quad \frac{5.1}{19} \quad \frac{5.4}{11} \quad \frac{6.7}{9} \quad \frac{6.2}{7} \quad \frac{5.7}{2} \quad 6.0 \quad \frac{6.3}{4} \quad \frac{5.5}{6} \quad \frac{5.1}{10} \quad \frac{5.4}{17} \quad \frac{6.4}{25}$$

3+0 + 1221.99 - Elev. Berms -

188+0
T.P. 7.27 1225.60 3.66 1218.33

189+0

190+0
T.P. 13.10 1227.195 1.505 1224.095

191+0

191+74

192+0
T.P. 2.49 1234.585 5.10 1232.095

193+0

193+N E of 12" C.I.P.

194+0
T.P. 5.86 1239.216 2.35 1233.35

195+0

5. 4 N. 28

$\frac{4.3}{25} \frac{5.1}{14} \frac{\sqrt{7.2}}{7} \frac{4.6}{5} 3.8 \frac{4.3}{5} \frac{5.2}{15} \frac{5.8}{25}$

$\frac{4.7}{25} \frac{5.3}{15} \frac{6.3}{11} \frac{6.5}{6} 5.7 \frac{6.1}{7} \frac{6.3}{13} \frac{6.9}{19} \frac{7.3}{22} \frac{7.7}{25}$

$\frac{0.3}{25} \frac{0.2}{14} \frac{3.2}{10} \frac{2.3}{3} 2.6 \frac{3.0}{7} \frac{1.1}{9} \frac{0.5}{12} \frac{1.1}{19} \frac{2.3}{23} \frac{2.7}{25}$

$\frac{2.9}{25} \frac{3.3}{21} \frac{5.1}{12} \frac{7.1}{9} \frac{7.3}{8} \frac{7.3}{4} 7.6 \frac{7.8}{2} \frac{5.6}{6} \frac{5.4}{13} \frac{7.4}{25}$

$\frac{1.3}{25} \frac{1.7}{21} \frac{2.6}{12} \frac{3.9}{10} \frac{3.1}{3} 3.6 \frac{4.2}{4} \frac{3.3}{6} \frac{3.9}{16} \frac{5.1}{25}$

$\frac{1.5}{25} \frac{1.9}{20} \frac{3.1}{13} \frac{4.4}{10} \frac{4.0}{2} 4.2 \frac{4.6}{3} \frac{4.9}{4} \frac{3.9}{6} \frac{3.7}{9} \frac{4.0}{18} \frac{4.8}{25}$

$\frac{5.7}{25} \frac{5.8}{18} \frac{6.0}{10} \frac{5.4}{6} 5.2 \frac{5.3}{7} \frac{7.3}{25}$

$\frac{6.4}{16} \frac{6.5}{14} \frac{6.7}{8} \frac{6.4}{8} \frac{5.4}{6} 5.0 \frac{5.3}{7} \frac{7.0}{9} \frac{8.0}{25}$
F.L.

$\frac{2.4}{25} \frac{2.8}{12} \frac{3.7}{8} \frac{4.7}{5} 4.2 \frac{4.0}{2} \frac{4.4}{7} \frac{4.6}{8} \frac{4.0}{9} \frac{1.8}{15} \frac{2.4}{25}$

$\frac{3.4}{25} \frac{3.4}{19} \frac{3.3}{6} \frac{6.0}{3} 4.5 \frac{4.0}{5} \frac{4.5}{11} \frac{3.3}{13} \frac{3.3}{29} \frac{2.8}{25}$

Sta + H.I. - Elev Rem's
196+0 1239.21

196+50± Edge of Pavc S. Route #44

196+50± E of Pavc S.R. #44

T.P. 0.375 1234.595 4.99 1234.22

T.P. 1.66 1224.84 11.415 1223.180

B.M. 5.27 1219.57 Nail in
Given B.M. Elev. 1219.58 Stump
check -.01 18" Maple
144+18
S.R. #44

5. $\frac{2.0}{25}$ $\frac{3.9}{4}$ 5.4 $\frac{5.5}{12}$ $\frac{5.8}{14}$ $\frac{3.7}{20}$ $\frac{3.7}{25}$ N 29

$\frac{4.28}{14}$ 4.82 $\frac{5.7}{23}$

$\frac{4.12}{17}$ 4.65 $\frac{5.53}{23}$

Wilson's Corners

North Sept 7, 1929 Fair

J. Gold Jr.
J. Merritt
H. Barton 30

Sta	+	H.I	-	Elev Remis
	5.54	1277.98		1272.44

B.M.

0+0

1+0

T.P.	2.05	1276.50	3.53	1274.45
------	------	---------	------	---------

2+0

3+0

T.P.	3.21	1267.11	12.60	1263.90
------	------	---------	-------	---------

4+0

5+0

T.P.	5.28	1265.98	6.41	1260.70
------	------	---------	------	---------

5+50

East

Elev

West

1270.90

$$\frac{0.5.0}{27'}$$

1269.39

$$\frac{0.4.0}{25.5'}$$

$$\frac{0.2.0}{22'}$$

1267.88

$$\frac{0.5}{19.0'}$$

$$\frac{0.1.0}{20.5'}$$

1266.37

$$\frac{F.1.0}{17'}$$

$$\frac{0.5}{18.5'}$$

1264.86

$$\frac{F.1.0}{17.5'}$$

$$\frac{F.1.0}{18.5'}$$

1263.35

$$\frac{F.1.5}{17.0'}$$

$$\frac{0.5}{18.5'}$$

1262.60

$$\frac{F.1.0}{17.5'}$$

Sta	+	H.I.	-	Elev. Rem's	East	± Elev. 3	West
		1265.98					

6+0					$\frac{Gr.}{20'}$	1261.70	$\frac{Gr.}{18.5'}$
T.P.	4.12	1258.62	11.48	1254.50			

7+0					$\frac{Gr.}{18.5'}$	1259.90	$\frac{F.I.0}{17.5'}$
-----	--	--	--	--	---------------------	---------	-----------------------

8+0					$\frac{F.I.0}{18'}$	1258.10	$\frac{F.I.5}{18.0'}$
-----	--	--	--	--	---------------------	---------	-----------------------

9+0					$\frac{C.I.0}{21'}$	1256.30	$\frac{Gr.}{17.5'}$
T.P.	4.22	1255.26	7.58	1251.04			

10+0					$\frac{C.I.0}{23'}$	1254.50	$\frac{C.I.0}{24.0'}$
------	--	--	--	--	---------------------	---------	-----------------------

11+0					$\frac{C.I.0}{22.5'}$	1250.0	$\frac{C.I.0}{26.0'}$
------	--	--	--	--	-----------------------	--------	-----------------------

B.M.	5.60	1249.66					
------	------	---------	--	--	--	--	--

(665) B.M.
 Spike
 in E Root
 60" Maple
 W. 85°
 Sta 11+75
 El. 1249.66

Sept. 9, 1929

Sta + H.I. - Elev. Reim's

B.M. 3.725 1253.39

11+50

1249.665 5 Mike in

E. Road
W-85
60 Maple St 11+75
El. 1247.665

12+0

1246.4

13+0

1235.6

14+0

1228.4

+50

1225.5

15+0

1224.0

16+0

1222.4

17+0

1220.8

+50

1220.0

18+0

1219.7

B.M.

1220.99 X on SW

19+0

Corner
E. Hill
Eul. Sta
19+30.9
El. 1220.99

Checking B.M.'s
Stopped on acct of
of Rain at 11:00 A.M.

Wilson's Corners N.

East RAIN E. Gr. El.

30
S. Gold Jr
S. Merritt
4 Barton

Sept 10, 1924 Fair

Wilson's Corners

S. Golden
S. M. ...
West 33'

5+2	+ H. 1	-	Elev	Remains
B.M.	3.495	1253.16	1249.65	Nail in
12+0				F. Root 45' Man An. 80'
T.P.	0.885	1241.765	12.28	1240.88 Sta 11+7.5 Elev 1243.065
13+0				
T.P.	2.155	1231.17	11.75	1230.015
14+0				
14+50		C.G.		
15+0				
T.P.	1.015	1225.53	7.665	1224.515
16+0				
B.M.		4.605	1220.915	(96)
17+0				
150		C.G.		
18+0				
19+0				
T.P.	8.585	1229.505	4.60	1220.92
20+0				

East		E. Gr. E. 1/8	West 33'
C. 2.5		1242.8	C. 2.0
24'			23'
F. 1.5		1235.6	C. 2.0
17.5'			23.3'
Grade		1228.4	F. 1.0
19'			17.5'
C. 0.5		1225.5	F. 1.0
20'			18.5'
C. 0.5		1224.0	F. 1.5
20'			18'
F. 1.0		1222.4	F. 2.5
18.5'			18'
F. 0.5		1220.8	F. 2.0
19.5'			17'
Gr		1220.0	F. 1.0
19.5'			18'
F. 0.5		1219.7	F. 0.5
19.3'			19'
F. 1.0		1219.13	F. 1.0
19.3'			18.5'
Gr		1219.90	F. 1.5
19'			17.3'

Sta	+	H.I	-	Flev. Rem's	East	Gr. Elev.	West
		1229.506					

20+50		C Grade				1220.76	
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21+0					$\frac{F. 0.5}{19'}$	1222.6	$\frac{C. 1.0}{21'}$
------	--	--	--	--	----------------------	--------	----------------------

22+0					$\frac{C. 1.5}{22'}$	1226.6	$\frac{C. 0.5}{21'}$
------	--	--	--	--	----------------------	--------	----------------------

T.P. 10.78 1238.89 1.395 1228.110

23+0	change	1/2:1 slope	to	1/4:1	$\frac{C. 7.5}{27'}$	1230.6	$\frac{F. 0.5}{19.5}$
------	--------	-------------	----	-------	----------------------	--------	-----------------------

24+0					$\frac{C. 0.5}{19.5}$	1233.48	$\frac{F. 3.0}{17.5}$
------	--	--	--	--	-----------------------	---------	-----------------------

25+0					$\frac{F. 0.5}{19.1}$	1230.35	$\frac{F. 1.0}{18.5}$
------	--	--	--	--	-----------------------	---------	-----------------------

T.P. 9.04 1229.85

Sept 11, 1929

Sta + H.I. - Elev. Points

T.P. 4.00 1233.85 1239.85

26+0

27+0

T.P. 10.83 1242.43 2.25 1231.60

28+0

29+0

T.P. 8.41 1248.93 1.91 1240.52

30+0 (Grade changed to save trees)
slope on W.S. 1:1

31+0 Change slope on E.S. 1 1/4:1

T.P. 6.695 1248.195 7.43 1241.5

32+0 Top of Bank on W side 15.71

33+0 Change on E side to 1:1

34+0 slope 1:1 on E.S. of Rd.

cloudy Wilson's corners N

Elev. f

Grad. Elev

F. 1.5
17.71 1232.6

F. 2.5
17' 1232.6

C. 0.5
20.5 1231.6

F. 0.5
18' 1232.6

G.F.
19.7 1234.1

C. 2.0
C. 3.5
23.3 (1239.8 Used)
1238.6

C. 2.0
22' (1243.075 Used)
1242.88

F. 3.5
18.5 1242.8

C. 2.0
20.3 1242.0

C. 3.5
22.0 1241.2

F. 8.0
18.5' 15.7'
Top of Bank
E. 0.5
20.0

C. 1.0
21.5

West 35

Sta + - - - Elev. Points
 1248.195

35+0

$\frac{C.1.0}{20.7'}$

1240.4

$\frac{F.1.0}{18.5'}$

36+0

$\frac{F.1.5}{17.7'}$

1240.45

$\frac{Gr.}{19'}$

37+0

$\frac{F.2.0}{16'}$

1242.2

$\frac{F.2.0}{17'}$

T.P. 11.15 1253.73 S.615 1242.58

38+0

$\frac{C.1.0}{20.5}$

1244.8

$\frac{F.0.5}{19.3}$

39+0

$\frac{Gr.}{19'}$

1247.4

$\frac{F.1.0}{18.5}$

40+0

$\frac{C.2.5}{22.3}$

1250.0

19.7

41+0

$\frac{C.1.0}{21.3}$

1250.75

$\frac{F.1.0}{18.7}$

42+0

$\frac{C.1.5}{22.3}$

1249.65

$\frac{F.0.5}{18.9}$

T.P. 8.96 1258.115 4.575 1249.155

43+0

$\frac{F.2.5}{16.9}$

1251.14

$\frac{F.3.0}{17.9}$

Sep 12, 1929

Sta	+ H.I.	- Elev. Points	Elev. Points
B.M.	7.41	1259.56	1252.15
44+0			
45+0			
T.P.	10.615	1263.22	1251.95
46+0			1257.61
47+0			
48+0	Change slope on E.S. to 1/4.1		
49+0		1267.30	1263.35
T.P.	3.95	1266.30	4.875
50+0			1262.35
51+0			
52+0			

Wilson's Corners N. Fair

3 Gold St
3 Merritt St
N Barton

East	Gr Elev	West
$\frac{F. 2.0}{46.7'}$	1253.74	$\frac{F. 0.5}{19'}$
$\frac{C. 0.5}{20.7'}$	1256.34	$\frac{Gr.}{20.0'}$
$\frac{C. 1.0}{21.3'}$	1258.67	$\frac{F. 0.5}{19'}$
$\frac{C. 3.5}{24.5}$	1260.44	$\frac{C. 1.0}{21.5}$
$\frac{C. 4.5}{24.3}$	1261.67	$\frac{Gr.}{22.5}$
$\frac{C. 3.0}{23.9'}$	1262.35	$\frac{C. 1.0}{21.5}$
$\frac{C. 0.5}{20.7}$	1262.47	$\frac{F. 1.5}{18}$
$\frac{F. 0.5}{18.7}$	1262.04	$\frac{F. 2.0}{17.5}$
$\frac{Gr.}{19.3}$	1261.34	$\frac{F. 1.5}{17.5}$

Sta	+	H.I.	-	Elct. Rem's
		673		
		1266.3		
53+0		674		5964
T.P.	3.10	1261.74	7.66	1258.64
54+0				
55+0				
56+0				
57+0		738		5120
T.P.	0.18	1256.38	5.54	1256.20
58+0				
59+0				
60+0				
61+0				

EZSA	Gr Elev's	West
$\frac{F.2.0}{17.1'}$	1260.64	$\frac{F.2.0}{17.5'}$
$\frac{F.1.0}{18.3'}$	1259.94	$\frac{F.1.5}{18.7'}$
$\frac{F.2.0}{17.1'}$	1259.24	$\frac{F.2.0}{17.5'}$
$\frac{F.1.5}{17.7}$	1258.54	$\frac{F.1.5}{17.3}$
$\frac{F.1.0}{18.9}$	1257.68	$\frac{F.1.0}{18}$
$\frac{F.1.0}{17.9}$	1255.84	$\frac{F.1.0}{17.9}$
$\frac{F.1.5}{17.3}$	1253.84	$\frac{F.1.0}{17.9}$
$\frac{F.1.0}{18.1}$	1251.84	$\frac{F.1.5}{17.1}$
$\frac{F.0.5}{18.9}$	1249.84	$\frac{F.1.0}{18.7}$

1256.38

Sta	+	H. ^{1256.38} ₁₂₅₃₇	-	Elev ^{1248.84} _{1248.84}	Rem's
T.P.	2.53	1251.37	7.54	1248.84	

62+0					
T.P.	4.18	1244.83	10.72	1240.65	

63+0

64+0

65+0

66+0

67+0

68+0

East

Gr Elev

West

F. 2.0
<u>18.7</u>

1247.27

Gr
<u>21.7</u>

1241.28

1236.6

1233.8

1231.0

1228.2

1225.4

Sta + H.I. - Elev Ref

B.M. 8.455 1245.835 1237.46

64+0

Ditch Bot 16'

63+0

Ditch Bot 16'

T.P. 11.825 1253.50 4.18 1241.675

62+0

16" Bottom

61+0

60+0

East

F.0.5

20.91

C.0.5

22.1

F.1.0

19.5

C.0.5

20.5

Gr El.

1236.6

1241.28

1247.27

1249.84

1251.84

West

Gr

21.1'

C.3.0

26'

C.1.5

23.8'

Gr

20.1

Sept 14 - 1929

Sta + H.I. - Elev Rem's

T.P. 6.405 1256.245 1249.84

60+0

59+0

T.P. 8.09 1261.435 2.90 1253.345

58+0

57+0

56+0

T.P. 6.95 1265.21 3.175 1258.260

55+0

54+0

53+0

52+0

Wilson's Corners N Cloudy

East Elev $\frac{E}{15}$

G. G. J. Jr.
S. H. H. H.
H. Barton
West #3

$\frac{Gr}{19.5}$

1251.84

$\frac{F.O.S}{18.5}$

$\frac{F.O.S}{18.9}$

1253.84

$\frac{Gr}{19.5}$

$\frac{Gr}{19.7}$

1255.84

$\frac{Gr}{19.3}$

$\frac{Gr}{19.7}$

1257.68

$\frac{Gr}{19.5}$

$\frac{F.O.S}{19.1}$

1258.54

$\frac{F.1.0}{18.7}$

$\frac{F.1.0}{18.3}$

1259.24

$\frac{F.1.0}{18.0}$

$\frac{Gr}{20.1}$

1259.94

$\frac{F.O.S}{18.7}$

$\frac{F.O.S}{18.9}$

1260.64

$\frac{F.1.0}{18.5}$

$\frac{C.1.0}{20.7}$

1261.34

$\frac{F.O.S}{19}$

Sta + HI - Elev. Reim.

1265.21

51+0 T.P. 6.15 1268.53 2.83 1262.38

50+0

Continued from page #

B.M. 0.68 1238.08 1237.40

65+0

66+0 T.P. 2.18 1232.90 7.36 1230.72

67+0

68+0

69+0

70+0

East ELEV'S West

$\frac{C.0.5}{20.5}$ 1262.04 F.1.5
18.3'

$\frac{C.1.5}{22}$ 1262.47 F.0.5
19.3'

$\frac{F.1.0}{18.5}$ 1233.8 F.1.0
18.5'

$\frac{C.1.5}{21.1}$ 1231.0 F.1.0
18.5'

$\frac{C.2.0}{22.5}$ 1228.2

$\frac{C.2.0}{21.9}$ 1225.4 C.0.5
20.5'

1222.80

1220.60

Dep. 16-29 Fair WINDON'S CORNER

Sta + H.I. - Elev Rems

T.P. 0.825 1226.725 1225.9

69+0

70+0

71+0

T.P. 2.095 1220.895 7.925 1218.80

72+0

73+0

74+0

T.P. 7.115 1221.615 6.395 1214.50

75+0

76+0

B.M. 2.23 1224.71 2.135 1219.48

77+0

N. 46045 J. Merritt & Barton 42

East Elev's West

C.I.V
21.1 1222.80 Gr
19.5'

C.O.V
20.1 1220.60 Gr
19.9

Gr
20' 1218.80 Gr
19.9'

Gr
20.1' 1217.40 F.O.V
19.3'

Gr
19.7' 1216.26 F.I.O
18.9'

Gr
19.5' 1215.51 F.I.O
18.3'

Gr
19.9' 1215.21 F.I.O
18.7

C.I.V
21.7 1215.36 C.O.V
20.7

C.I.V
22 1215.45 C.O.V
20.7

Sta + H.I. - Elev. Rem's
1221.71

78+0

T.P. 3.205 1215.95 9.32 1212.39

79+0

80+0

T.P. 3.39 1212.685 6.30 1209.295

81+0

82+0

83+0

B.M. 4.565 1213.435 3.815 1208.87 ⁽⁹⁴⁾ Sept 17

84+0

85+0

86+0

T.P. 11.365 1222.085 2.765 1210.72

Elev

C.O.S

20.7

F.O.S

18.7

C.I.O

19.3'

F.O.S

19.3'

F.I.O

18.1'

F.I.S

17.9'

F.2.0

17.5'

F.1.0

18.5

C.I.O

21.1

Elev's

1212.9

1210.35

1209.3

1208.7

1208.1

1207.5

1207.40

1208.3

1209.44

West

F.O.S

19.3

F.1.5

18.0

G.T.

20.3'

F.O.S

18.7'

F.1.5

17.9'

F.2.0

17.1'

F.1.5

17.9

F.O.S

19.3

G.O.S

20.3

St 2 + H.I. - Elev rem's
1222.085

89+0

88+0

89+0

T.P. 9.39 1228.54 2.935 1219.15

90+0

91+0

T.P. 7.23 1233.47 2.30 1226.24

92+0

93+0

B.M. 6.35 1227.15 ⁽²³⁾

94+0

T.P. 1.88 1225.72 9.575 1223.895

95+0

Elev

Elev's

West

C. 1.5
21.7'

1211.59

C. 1.0
21.1'

C. 0.5
20.3

1214.75

C. 1.0
21.0'

F. 1.05
18'

1218.05

F. 0.5
19.3'

C. 1.0
21.1'

1221.35

C. 1.0
21.9'

C. 1.0
21.1'

1224.65

C. 1.5
22.3'

C. 1.0
21.7'

1227.95

C. 1.0
21.3

C. 1.0
21.7'

1228.2

C. 1.0
21.5

1225.4

F. 1.5
17.9'

F. 2.0
17.1'

1222.6

F. 2.5
18'

S⁴/₂ + H.I. - Elev. Rem's
1226.775

96+0

97+0

98+0

T.P. 2.57 1218.49 9.85 1215.925

99+0

100+0

T.P. 1.695 1209.45 10.74 1207.755

101+0

Ditch
16" Bottom

102+0

1 1/2' Bot.

103+0

1 1/2' Bot.

104+0

B.M.

1 1/2' Bot.
9.45
4.86 1204.59 x one

East

Elev's

West

F. 0.5
19.3'

1219.96

C. 0.5
20.5'

C. 0.5
20.7'

1218.3

C. 2.0
22.7'

C. 2.5
23.7'

1216.22

C. 1.0
21.7'

C. 1.0
21.5'

1213.0

C. 2.0
23.3'

F. 2.0
17.0'

1209.61

F. 2.0
17.1'

F. 1.5
19.3'

1207.05

F. 2.0
18.9'

Gr.
21.1'

1205.31

F. 0.5
20.3'

Gr.
21.1'

1204.4

F. 1.0
19.7'

F. 2.0
16.9'

1203.9

F. 2.0
18.7'

Sept 18-79 Fair Wilson's Corns
 Sta + H.1 - Elev Remis
 B.M. 3.01 1207.60 1204.59

104+0 D 1 1/2' Bot. $\frac{F. 2.0}{16.9}$ 1203.9 $\frac{F. 2.0}{18.7}$

105+0 D 2' 6" Bot. $\frac{F. 2.5}{17.5}$ 1203.57 $\frac{F. 2.0}{19.5}$

106+0 D 2' 6" Bot. $\frac{F. 2.5}{17.5}$ 1203.63 $\frac{F. 2.0}{19.7}$

107+0 D 2' 6" Bot. $\frac{F. 2.0}{19.9}$ 1203.79 $\frac{F. 1.5}{20.3}$

108+0 Ditch 26" B. $\frac{C. 1.5}{24}$ 1203.89 $\frac{Gr}{23}$

T.P. 7.00 1211.35 3.25 1204.35

109+0 Eliminate wide ditch ^{ditch} $\frac{C. 5.0}{26.9}$ 1204.09 $\frac{C. 2.0}{25.5}$
 on East side ^{Bottom}

110+0 $\frac{F. 0.5}{19.1}$ 1205.6 $\frac{Gr}{19.9}$

111+0 $\frac{F. 1.5}{18}$ 1207.2 $\frac{F. 1.0}{19.3}$

112+0 $\frac{F. 2.0}{17}$ 1208.8 $\frac{F. 1.5}{17.9}$

46
 S. Ed Jr
 S. Harriet
 H. Barton
 East
 E Elev's
 West

$\frac{F. 2.0}{16.9}$ 1203.9 $\frac{F. 2.0}{18.7}$

$\frac{F. 2.5}{17.5}$ 1203.57 $\frac{F. 2.0}{19.5}$

$\frac{F. 2.5}{17.5}$ 1203.63 $\frac{F. 2.0}{19.7}$

$\frac{F. 2.0}{19.9}$ 1203.79 $\frac{F. 1.5}{20.3}$

$\frac{C. 1.5}{24}$ 1203.89 $\frac{Gr}{23}$

$\frac{C. 5.0}{26.9}$ 1204.09 $\frac{C. 2.0}{25.5}$

$\frac{F. 0.5}{19.1}$ 1205.6 $\frac{Gr}{19.9}$

$\frac{F. 1.5}{18}$ 1207.2 $\frac{F. 1.0}{19.3}$

$\frac{F. 2.0}{17}$ 1208.8 $\frac{F. 1.5}{17.9}$

Sta + H.I. - Elev. Rem

1211.35

113+0

T.P. 8.81 1217.70 2.46 1208.89

114+0

B.M. 7.885 1209.815

115+0

T.P. 9.02 1225.31 1.41 1216.29

116+0

117+0

118+0

T.P. 6.21 1228.82 2.70 1222.61

119+0

120+0

121+0

East

Elev.

West

F. 1.5
17.7'

1210.8

F. 0.5
19.5'

C. 0.5
20.5'

1212.33

F. 0.5
19.7'

C. 3.0
24.5'

1214.93

C. 2.5
23.3'

C. 2.0
22.7'

1218.2

C. 1.0
21.5'

C. 0.5
20.7'

1220.6

Gr.
20.1'

Gr.
19.5'

1221.8

Gr.
19.7'

F. 1.5
18.5'

1223.0

F. 0.5
19.1'

F. 1.0
18.3'

1224.2

F. 1.0
18.7'

F. 1.0
18.3'

1225.4

F. 1.0
18.7'

Sta + H.I. - ELEV. REHS
 1228.82

122+0
 T.P. 12.64 1238.94 2.52 1226.30

123+0

124+0
 B.M. 5.35 1238.85 5.44 1233.50
 (53)
 125+19

125+0

126+0
 T.P. 8.85 1245.58 2.12 1236.73

127+0

128+0

129+0

130+0

East ± ELEV. West

$\frac{F.O.S}{19.1'}$ 1226.8 $\frac{F.O.S}{19.5'}$

$\frac{Gr}{20.0'}$ 1228.6 $\frac{Gr}{19.9'}$

$\frac{Gr}{20.0'}$ 1230.8 $\frac{C.O.S}{19.9'}$

$\frac{C.O.S}{21.7'}$ 1233.4 $\frac{C.O.S}{20.5'}$

$\frac{C.O.S}{20.5'}$ 1236.8 $\frac{C.1.0}{21'}$

$\frac{C.O.S}{20.5'}$ 1239.75 $\frac{C.1.5}{22.5'}$

$\frac{F.O.S}{19'}$ 1241.8 $\frac{F.O.S}{19.3'}$

$\frac{Gr}{19.7'}$ 1242.3 $\frac{Gr}{20'}$

$\frac{C.O.S}{20.7'}$ 1242.68 $\frac{F.O.S}{19.7'}$

Sta	+	H.I.	-	Elev	Corr's	East	± Elev	West
T.P.	2.885	1245.545	2.92	1242.66				
131+0						$\frac{C.1.0}{21.1}$	1242.19	$\frac{C.0.5}{20.8}$
132+0						$\frac{C.1.5}{22.1}$	1240.8	$\frac{C.1.0}{21.1}$
133+0						$\frac{C.1.5}{22.5}$	1239.3	$\frac{C.0.5}{20.7}$
T.P.	1.685	1242.48	4.75	1240.795				
134+0						$\frac{C.0.5}{20.7}$	1237.8	$\frac{F.0.5}{19.3}$
B.M.			2.40	1240.08	(05)			
135+0						$\frac{F.1.0}{18.7}$	1236.3	$\frac{F.2.0}{17.0}$
T.P.	3.72	1239.02		1235.3				
136+0						$\frac{C.0.5}{20.5}$	1235.04	$\frac{F.0.5}{19.9}$
137+0						$\frac{F.0.5}{19.5}$	1235.25	$\frac{F.0.5}{18.9}$
T.P.	4.05	1238.80	4.27	1234.75				
137+70.73						$\frac{F.0.5}{19.1}$	35.89 1235.56	35.39 $\frac{F.1.0}{18.3}$
+95.73							35.51 1235.68	36.13

Sta + H.I. - Elev. Curve
 38.80
 Slope stakes along the
 138+0 curve are set on East
 Side only.

+20.73 P.C.

+45.73

+70.73

+95.73

139+0

+23.36

+48.36 P.T.

T.P. 8.99 1245.39 2.40 1236.40

+73.36

B.M. Established 3.75 1241.64

Spike in
 W. Root
 24" Maple
 Sta 143+0
 N. 81' 1/2

East E Elev. West

GI 35.53 1235.7 36.21 $\frac{F.1.0}{18.1'}$
 21.5

$\frac{F.0.5}{23.5'}$ 35.62 1235.79 36.60 $\frac{F.1.0}{18.5'}$

$\frac{F.0.5}{26.3'}$ 35.73 36.90 37.06

$\frac{F.1.0}{26.9}$ 35.85 36.02 37.54

35.96 36.13 37.65

$\frac{F.0.5}{27.0'}$ 35.98 36.15 37.64

$\frac{F.0.5}{26.3}$ 36.10 36.27 37.43 $\frac{F.1.0}{19'}$

GI 36.23 36.40 37.21 $\frac{F.0.5}{19.3}$
 24.3

$\frac{L.0.5}{22.3}$ 36.45 36.62 37.07 $\frac{F.0.5}{19.3}$

Sept. 24 (Fair) Wilson's

5/2 + H. 1 - Elev. 1244.24
B.M. 2.60 1244.24 1241.64

139+98.1

140+0 Check Grade Stake on N. Side

141+0

142+0

143+0 Slopes on S. Side 1:1 (Slope Stake Set
T.P. 3.97 1245.61 2.60 1241.64 Flahon Top of Bank)

144+0

T.P. 2.895 1241.70 6.805 1238.805

145+0

146+0

147+0

Corners N
North

Elev's

S. Gold Jr.
S. Merritt
H. Barton South

1236.83

C. 0.5
20.3'

1236.86

C. 1.0
21.3'

C. 1.5
21.7'

1238.1

C. 1.5
21.9'

C. 1.5
22.5'

1239.6

C. 1.5
21.9'

C. 1.0
21.1'

1240.35

C. 2.0
19'

Gr.
19.9'

1239.6

Gr.
20.1

Gr.
18.7'

1238.1

C. 1.0
21.1'

F. 1.5
17.9'

1236.5v

Gr.
20.3'

F. 1.5
17.5'

1234.5

Gr.
19.7'

Sta	+	H.I.	-	Elev	Rem's
				1241.70	
148+0					
T.P.	1.29	1230.94	12.05	1229.65	
149+0					
150+0					
151+0					
T.P.	3.525	1229.025	5.44	1225.50	
152+0					
B.M.		3.225		1225.80	(96)
153+0					
T.P.	4.30	1225.90	7.425	1221.60	
154+0					
155+0					
156+0					

52

North	Elev.	South
$\frac{F.2.0}{17.7'}$	1232.36	$\frac{G.F.}{19.7'}$
$\frac{F.1.5}{17.9'}$	1230.15	$\frac{G.F.}{20.3'}$
$\frac{F.1.5}{17.7'}$	1227.86	$\frac{G.F.}{20.3'}$
$\frac{G.F.}{19.7'}$	1225.50	$\frac{G.F.}{20.0'}$
$\frac{C.1.0}{21.1'}$	1223.22	$\frac{G.F.}{19.9'}$
$\frac{G.F.}{19.9'}$	1222.60	$\frac{F.1.0}{18.5'}$
$\frac{F.0.5}{19.7'}$	1222.26	$\frac{F.1.5}{17.7'}$
$\frac{G.F.}{19.5'}$	1222.24	$\frac{F.1.0}{18.3'}$
$\frac{G.F.}{19.3}$	1222.55	$\frac{F.1.5}{17.9'}$

Sept. 25 - Fair

Wilson's

Corners N.

S. Gold St.
S. Merritt
N. Barton

53

Sta + H.I. - Elev. Bemis

North

± Elev.

South

T.P. 6.21 1228.76 1222.55

15740

F.O.5
19.3'

1223.17

Gr.
20.1'

15840

F.O.5
19.0'

1224.12

C.1.5
22'

15940

T.P. 7.615 1233.425 2.95 1225.81

F.O.5
18.7'

1225.39

C.1.0
21.1'

16040

C.1.5
22'

1226.82

C.1.0
21.5'

16140

Gr.
20.5'

1228.40

Gr.
19.9'

16240

Gr.
19.1'

1228.70

F.O.5
19.7'

16340

T.P. 4.60 1231.65 6.375 1227.05

C.O.5
19.7'

1227.7

Gr.
19.9'

16440

F.1.0
18.7'

1226.7

Gr.
19.7'

16540

C.2.0
22.9'

1225.7

C.2.0
22.7'

Sta	+ 1231.65	- 4.1	Elev	Rem's	North	Elev	South
T.P.	5.50	1230.03	7.12	1224.53			
166+0	Change slopes on Both sides (1:1)				0.15	1223.30	0.25
					20.7'		21.5'
167+0	Change slopes on N Side to 1:1				0.15	1219.50	0.45
T.P.	6.235	1224.765	12.00	1218.03	20.3'		26.3'
168+0					0.1	1215.70	0.2.0
T.P.	7.46	1214.51	12.215	1212.05	19.0		23.5'
169+0					F. 2.0	1211.90	F. 1.5
					17'		17.9'
170+0	1.87	1208.765	7.615	1206.895	F. 0.5	1208.48	F. 0.5
					18.9'		18.5'
171+0					F. 1.0	1206.30	F. 1.0
					18.7'		18.7'
172+0					0.1	1204.50	F. 0.5
					19.5'		18.9'
173+0					0.1	1202.80	F. 0.5
					19.9'		19.3
174+0					0.1	1201.55	F. 0.5
B.M.					19.7'		19.3
				6.975	1201.79		

Sept 28, 1929 Fair Wilson

Carriers N.

S. Gold Jr.
J. Merritt
H. Barton } South

Sta	+ H	-	Elev. Re	13
B.M.	4.49	1206.28		1201.79
175+0				
T.P.	6.96	1206.81	6.43	1199.85
176+0				
T.P.	2.30	1196.12	12.99	1193.82
177+0				
178+0				
T.P.	7.405	1198.455	5.07	1191.05
179+0				
180+0				
T.P.	12.42	1209.595	1.28	1197.175
181+0				
182+0	Change slope on N side to 1:1			
183+0				
B.M.		2.585	<u>06.898</u>	1207.01

North	Elev	South
$\frac{C. 3.0}{24.0'}$	1199.35	$\frac{C. 0.5}{20.7'}$
$\frac{C. 4.0}{26'}$	1195.95	$\frac{C. 0.5}{20.5'}$
$\frac{F. 0.5}{19.0'}$	1191.71	$\frac{F. 1.5}{17.7'}$
$\frac{F. 2.0}{17.9}$	1190.45	$\frac{F. 2.0}{17.3}$
$\frac{F. 2.0}{18.0}$	1191.71	$\frac{F. 3.0}{18.4}$
$\frac{F. 1.0'}{18.1'}$	1196.0	$\frac{C. 1.5'}{22.3'}$
$\frac{C. 2.0'}{22.5}$	1200.50	$\frac{C. 2.0'}{22.7'}$
$\frac{C. 2.5'}{21.7'}$	1203.50	$\frac{C. 4.0}{25.5'}$
$\frac{F. 2.5}{17.3'}$	1203.50	$\frac{C. 2.0}{22.5'}$

Oct. 1, 1929 Wilson's Gormers

Sta + H.L. - Elev. Rem's

B.M. 0.745 1207.755 1207.01

184+0

T.P. 6.885 1209.815 4.825 1202.93

185+0

T.P. 12.03 1220.785 1.06 1208.765

186+0

187+0

188+0

T.P. 5.39 1222.285 3.79 1216.995

189+0

T.P. 8.485 1227.38 3.49 1218.895

190+0

T.P. 11.95 1238.31 1.02 1226.36

191+0

192+0 Change Slope on S. Side to 1:1

T.P. 10.425 1240.285 8.45 1229.86

N. (Fair)

North

Elev

F 3.0
18.3'

1202.54

F 1.5
17.5'

1204.80

C 3.0
24.3'

1209.80

G.F.
20.5'

1216.29

F 1.5
17.5'

1218.50

F 2.0
17.5'

1220.9

G.F.
20.7'

1223.5

C 1.0
21.3'

1230.0

G.F.
20.7'

1232.7

S. Gold Jr.
S. Merritt
H. Barton South

F 3.0
18.3'

F 1.5
17.5'

C 2.0
23'

C 1.0
21.1'

F 1.5
18.0'

F 0.5
19.5'

C 2.5
23.7'

C 4.5
26.3'

C 3.0
21.7'

Sta + H.I. - Elev. Rem.
 1240.285

193+0

194+0

195+0

196+0

T.P. 0.305 1233.56 7.03 1233.255
 T.P. 6.10 1227.05 12.61 1220.95
 B.M. 7.34 1219.71

North) @ Elev. South

F. 4.0
 19.7' 1231.51

C. 0.5
 20.1' 1232.41

C. 1.5
 22.3' 1234.11

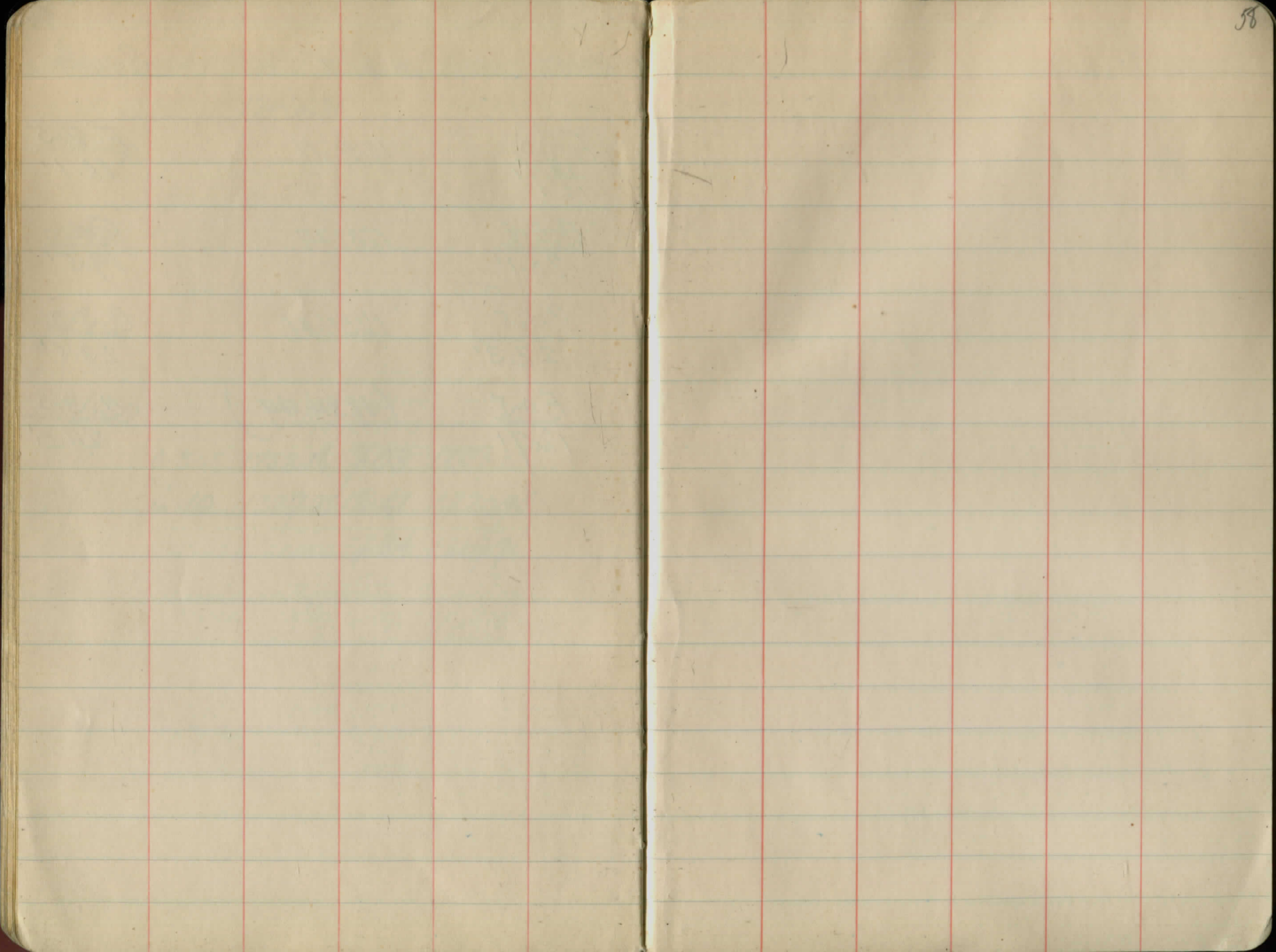
F. 0.5
 18.7' (1234.49)

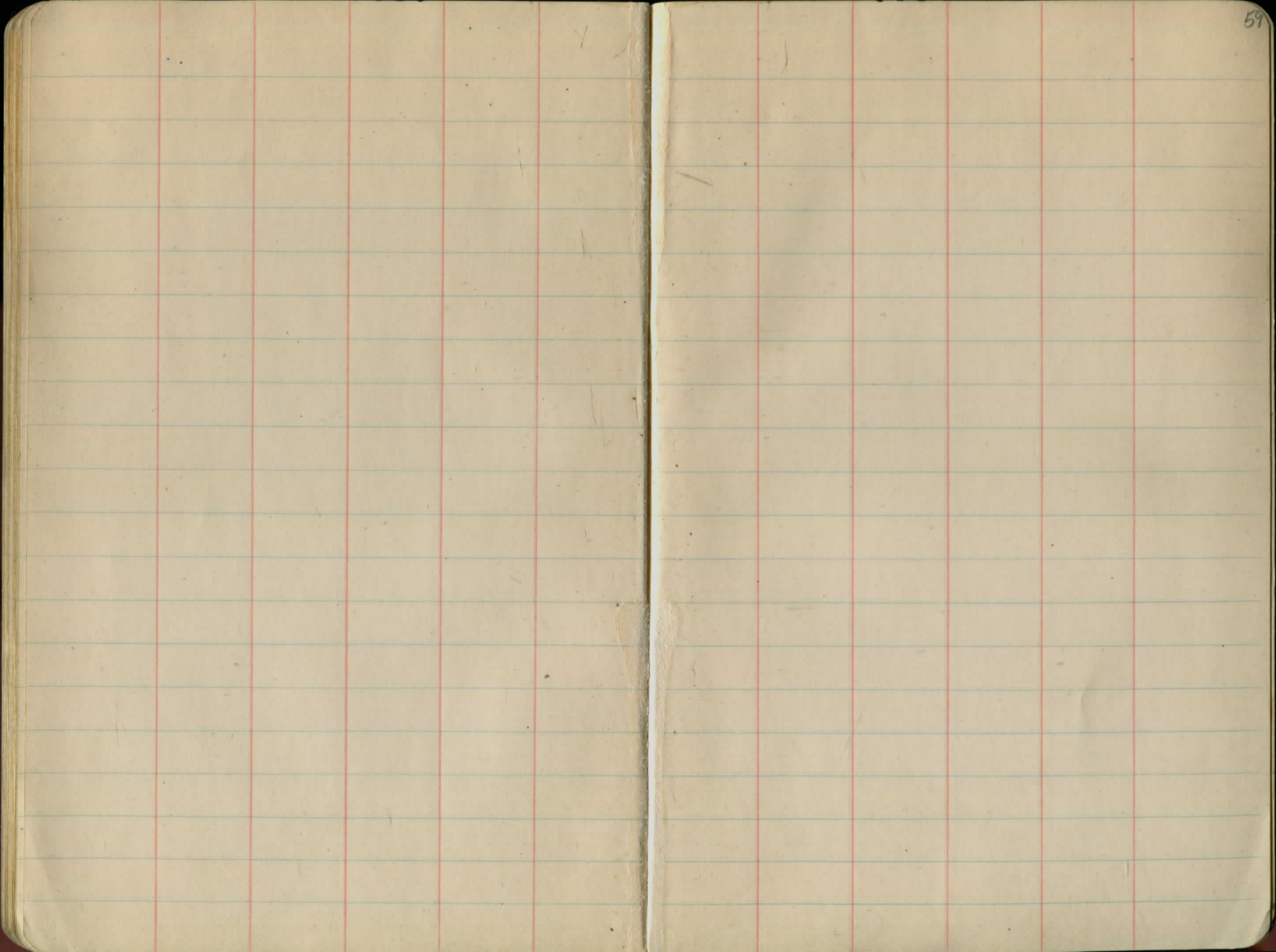
F. 2.5
 18.1'

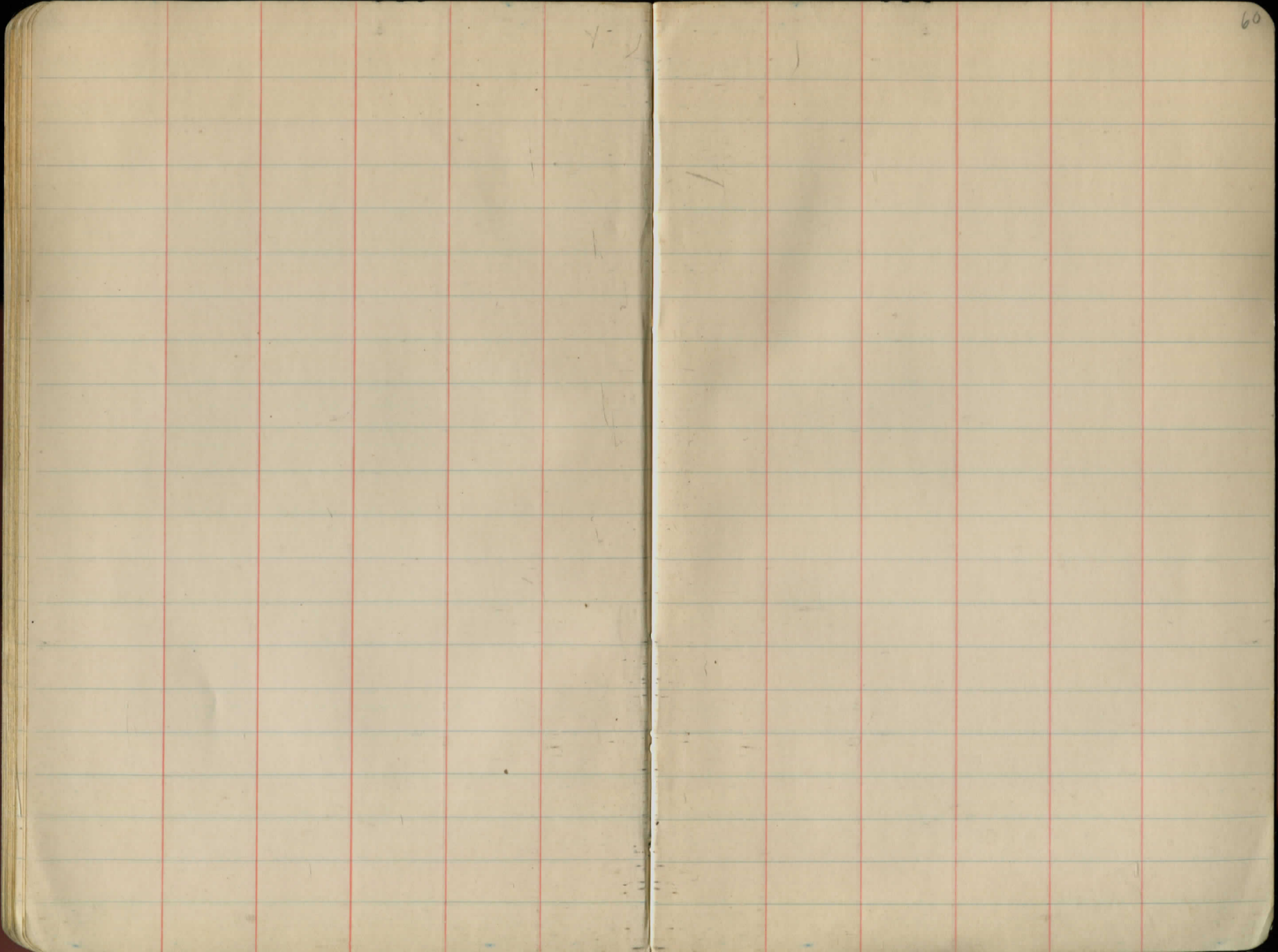
G.
 19.5'

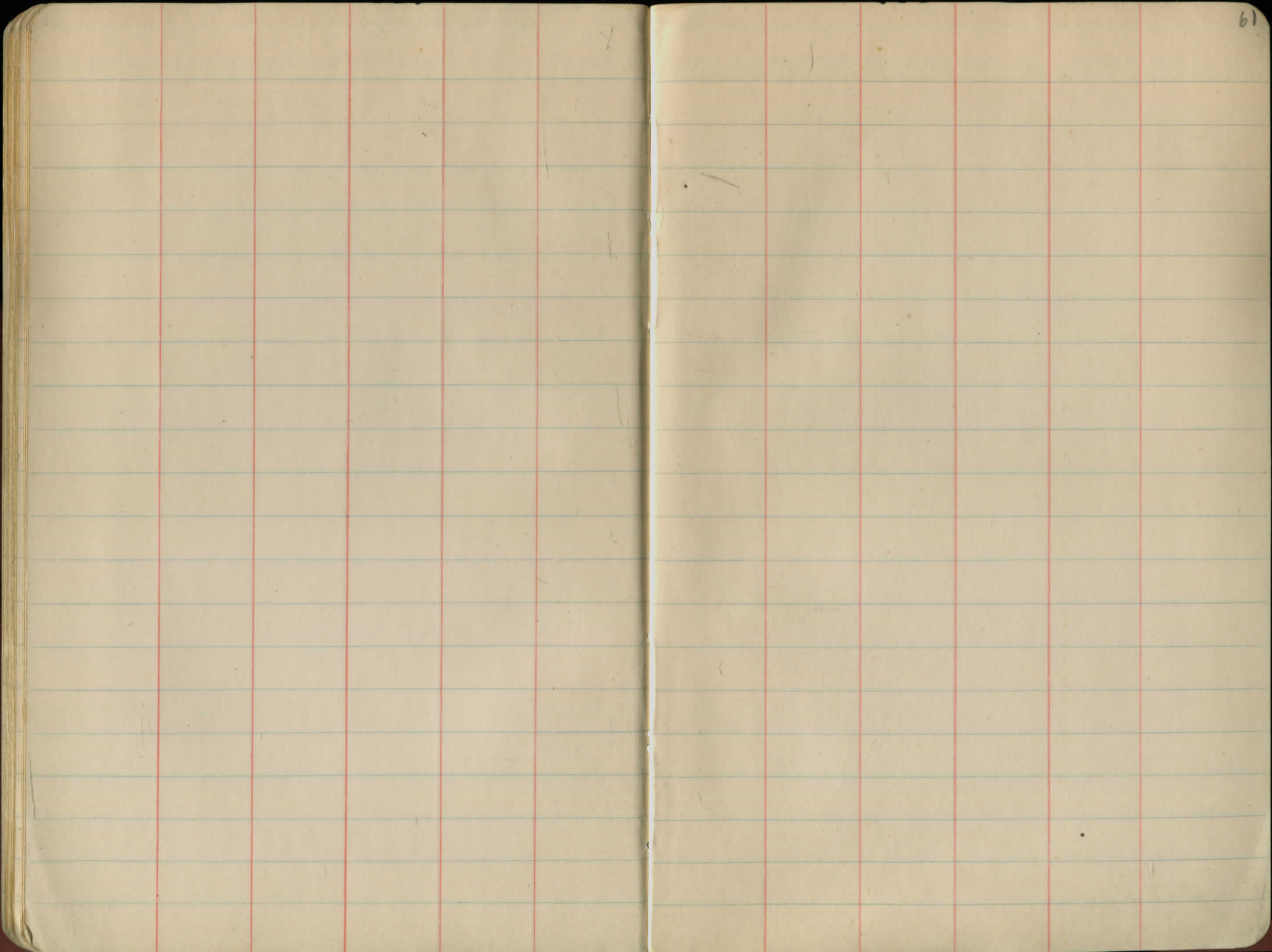
C. 3.0
 23.5'

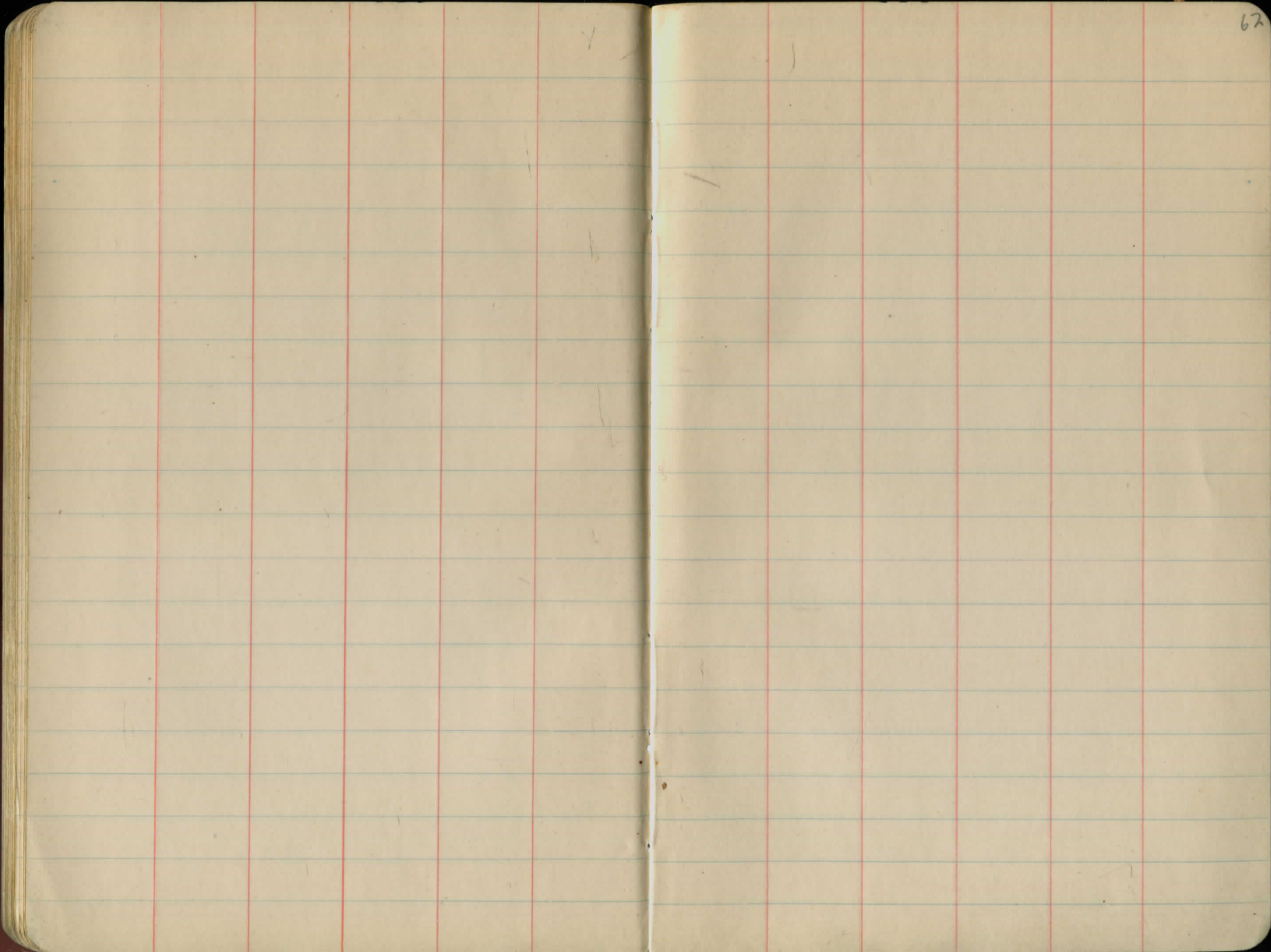
C. 3.0
 24.0'

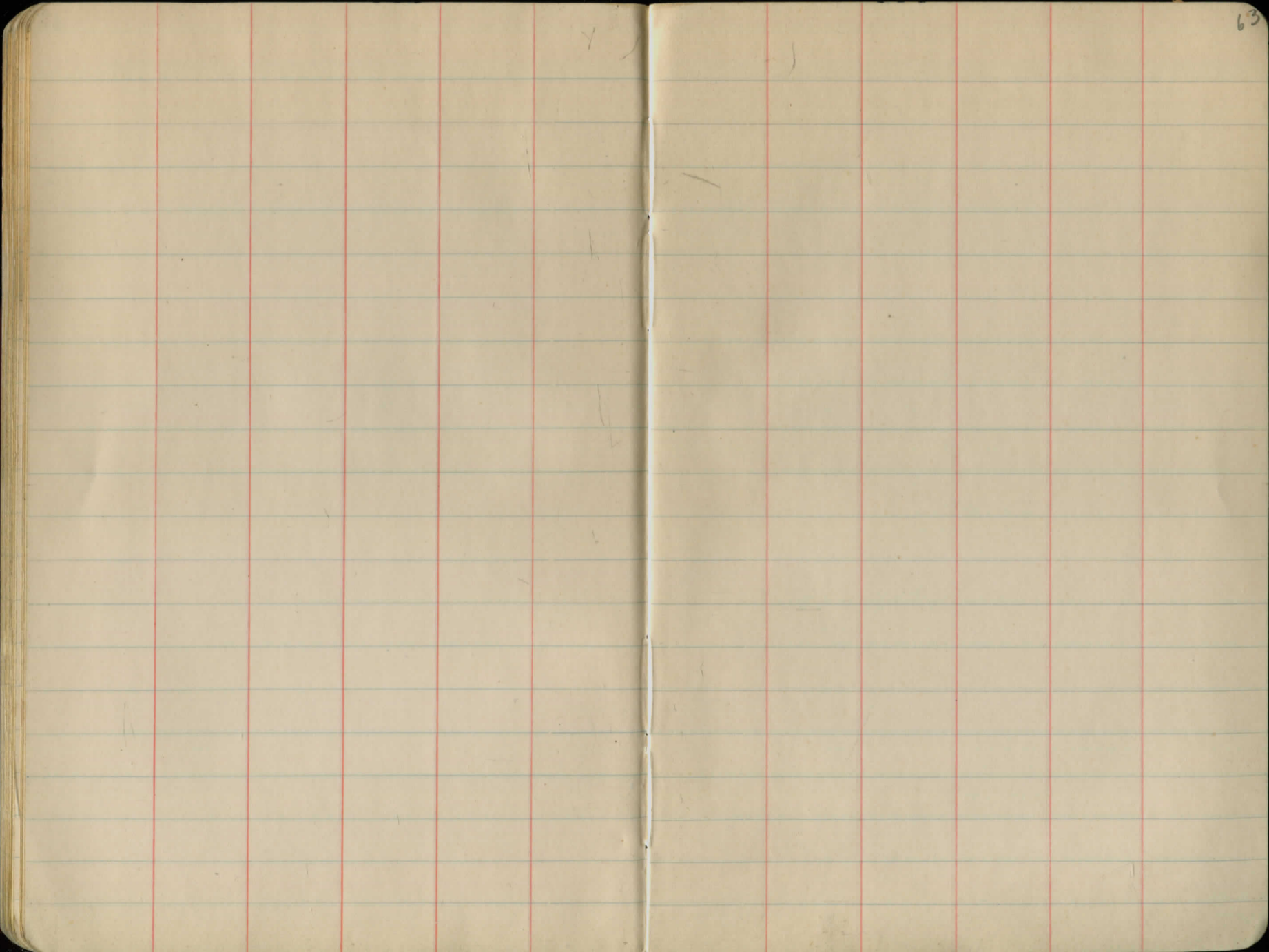


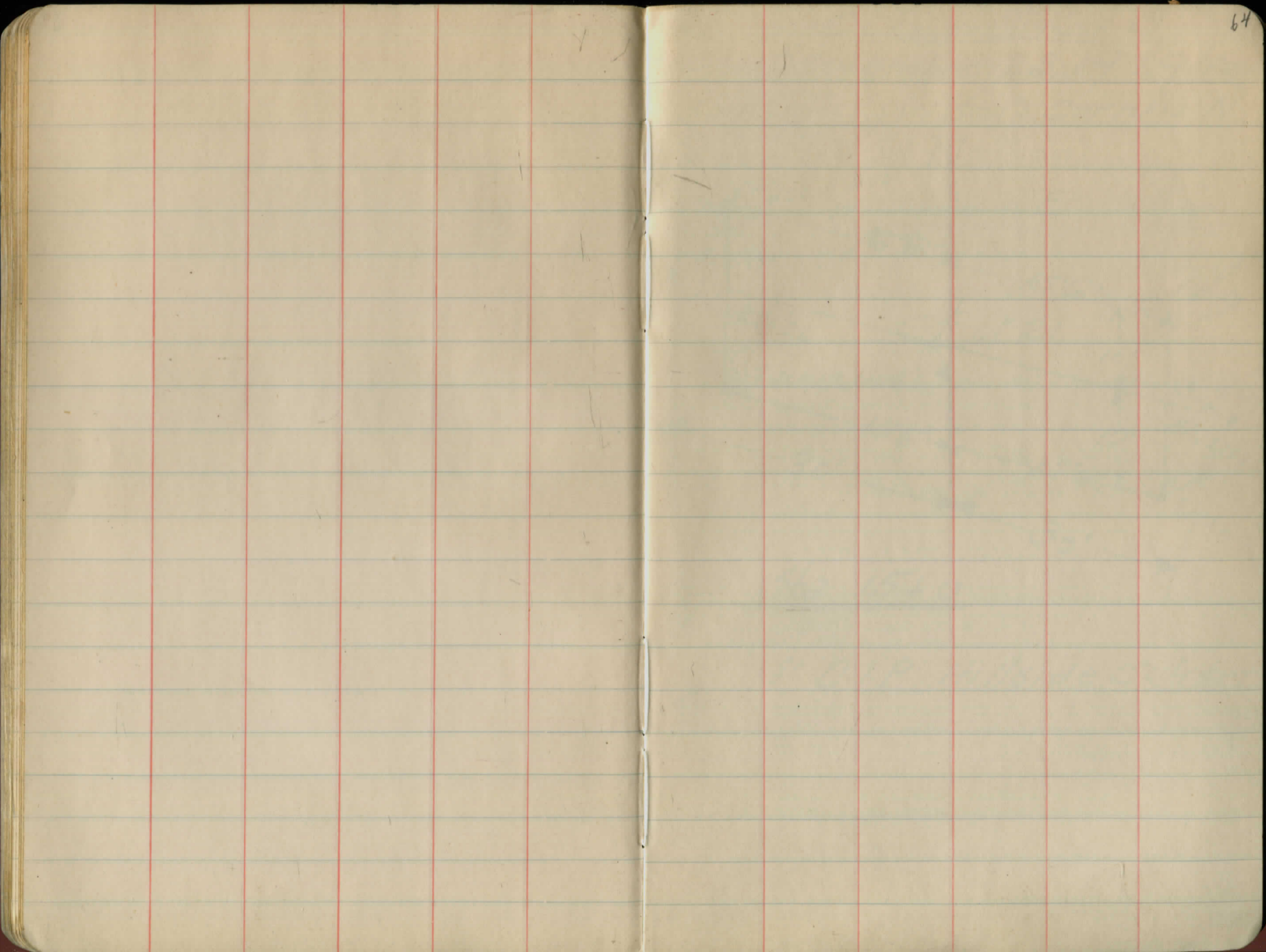








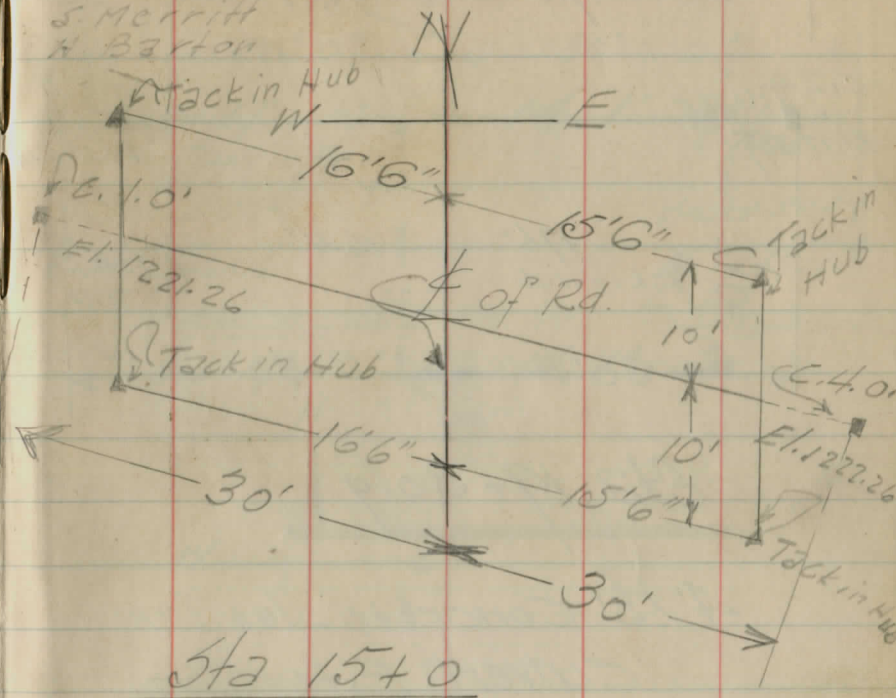




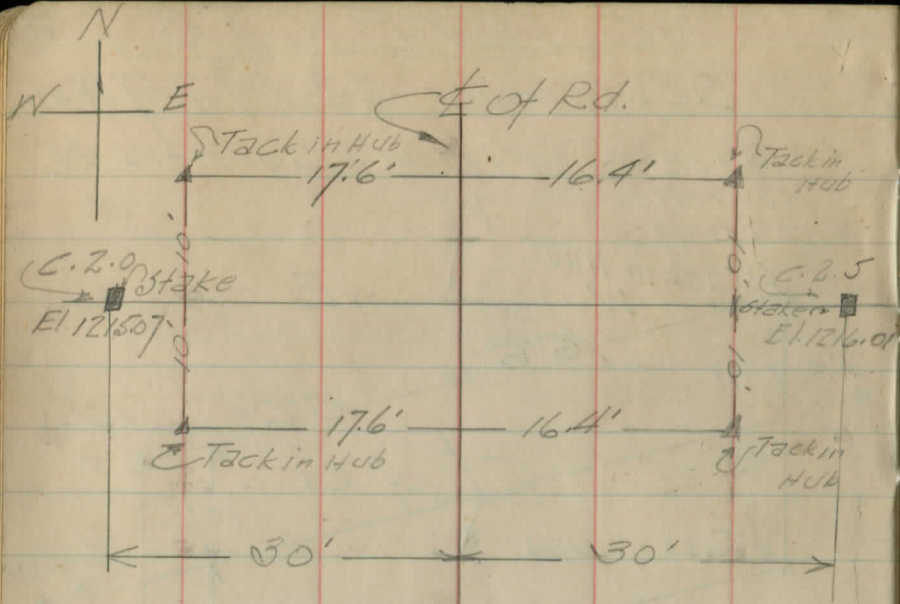
CULVERTS

September 23, 1929 (Fair)

J. G. Gold Jr. Wilson's Corners N.
S. Merritt
H. Barton



18" C.I.P. Hillside Culvert



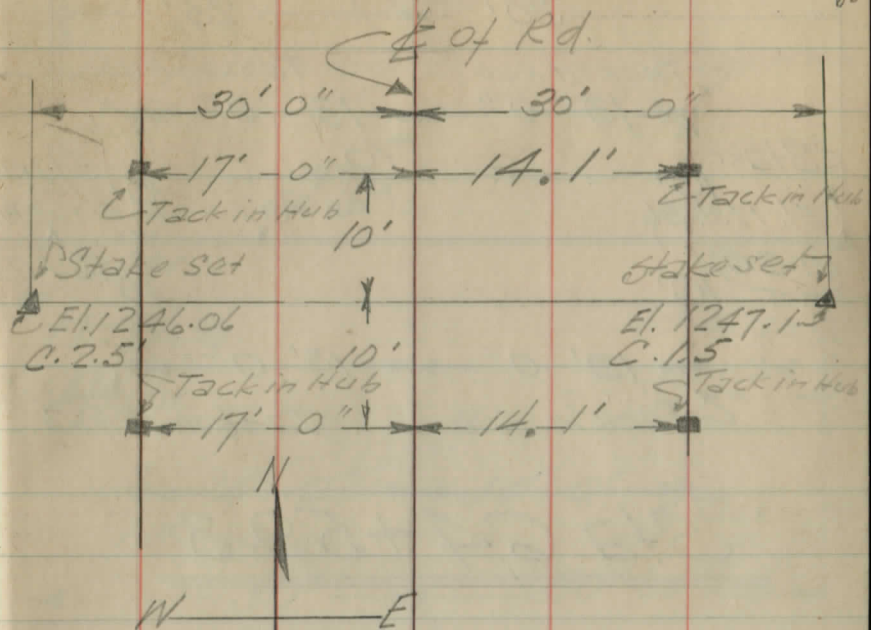
Sta 19+30.9

4' x 3' Concrete Slab Top
Culvert Extension

Clean Outlet Channel
(250')

(Stakes Set 1' offset)

Sept 30, 1929
cloudy
S. Gold Jr.
S. Merritt
H. Barton
66

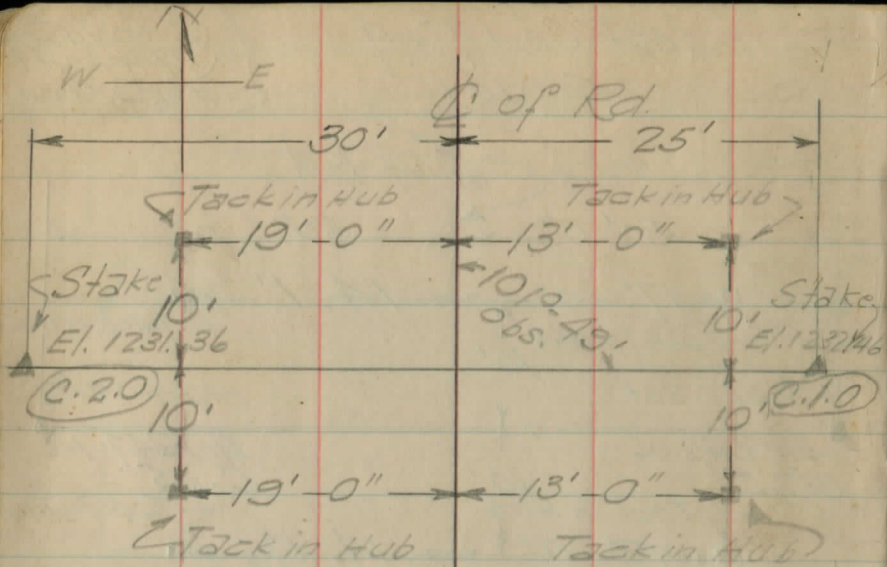


Sta 43+23

3' x 3' Slab Top Extension

Open Outlet Channel (for 150')

(Stakes Set 1' offset)

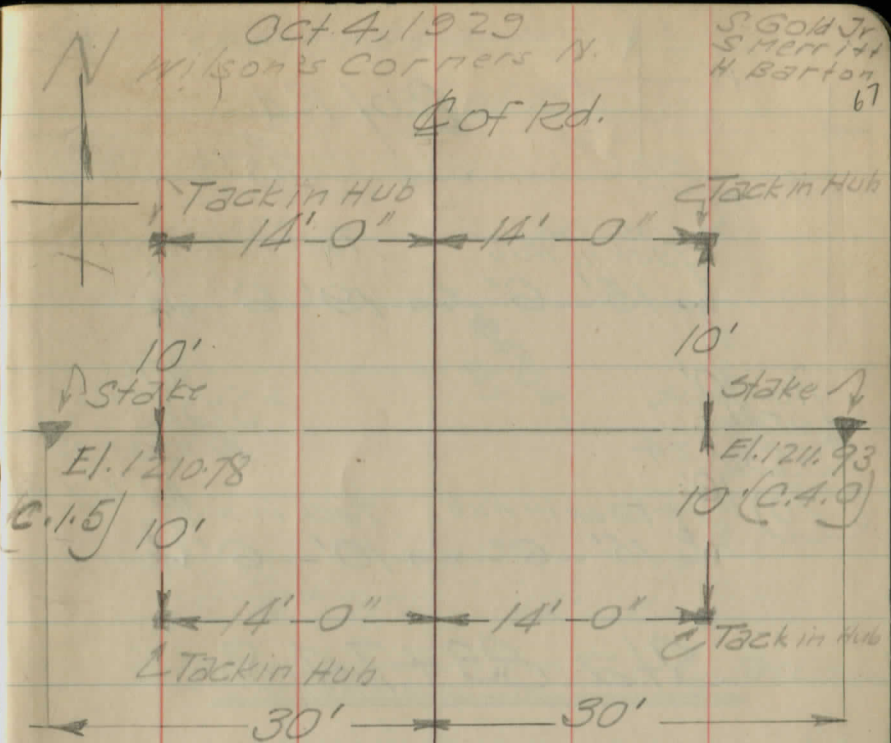


Sta 64+59.3

2 1/2' x 3' x 4 1/2" Slab Top Extension

- Hubs (with Tacks) on W. Side - 6' offset
- " " " " E. Side 1' " "

Note: The Outlet Channel to be
 Connected with the Rd. Ditch
 The W. Headwall to be removed
 & placed where required by
 the Engineer

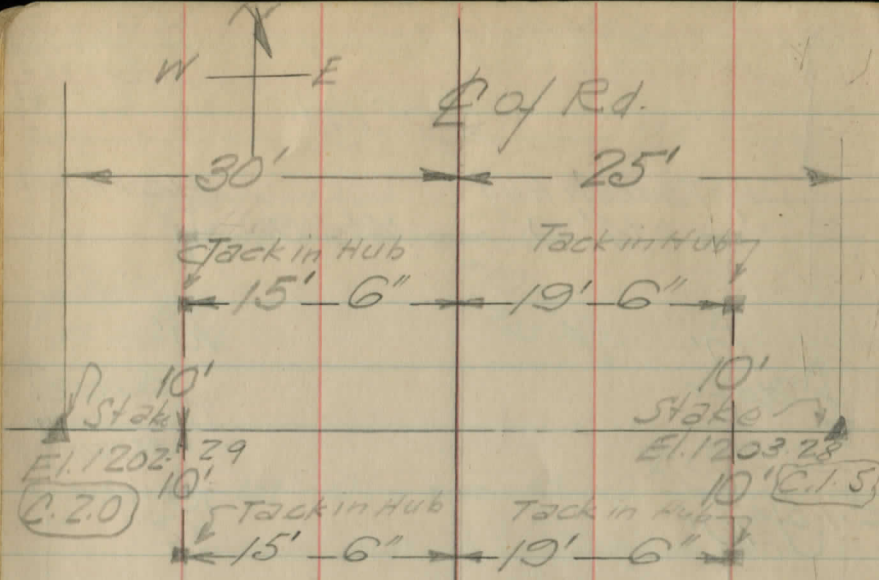


Sta 74+36.8

3' x 3' x 26' CONC. BOX
 CULVERT

- Hubs with tacks on E. Side 1 1/2' Offset
- " " " " on W. Side 1/2' " "

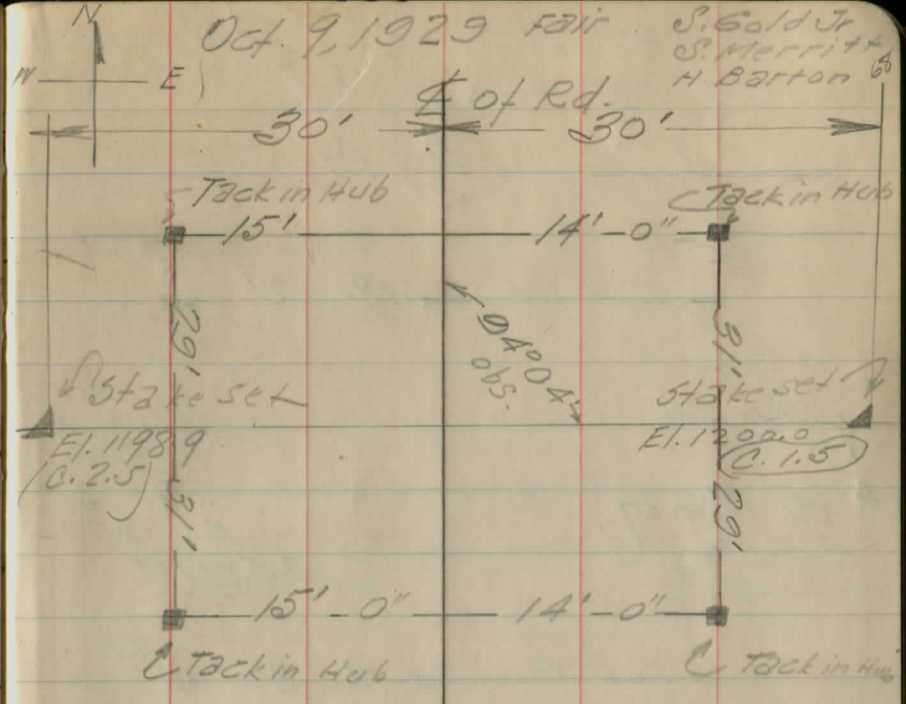
Oct 4, 1929
 Wilson's Corners N.
 S. Gold Jr.
 S. Merritt
 H. Barton
 67



Sta 83+74.8

4' x 3' x 28' CONC. BOX
CULVERT

Hubs with Tacks on E. Side 6' offset
 " " " " W. " " 1' offset

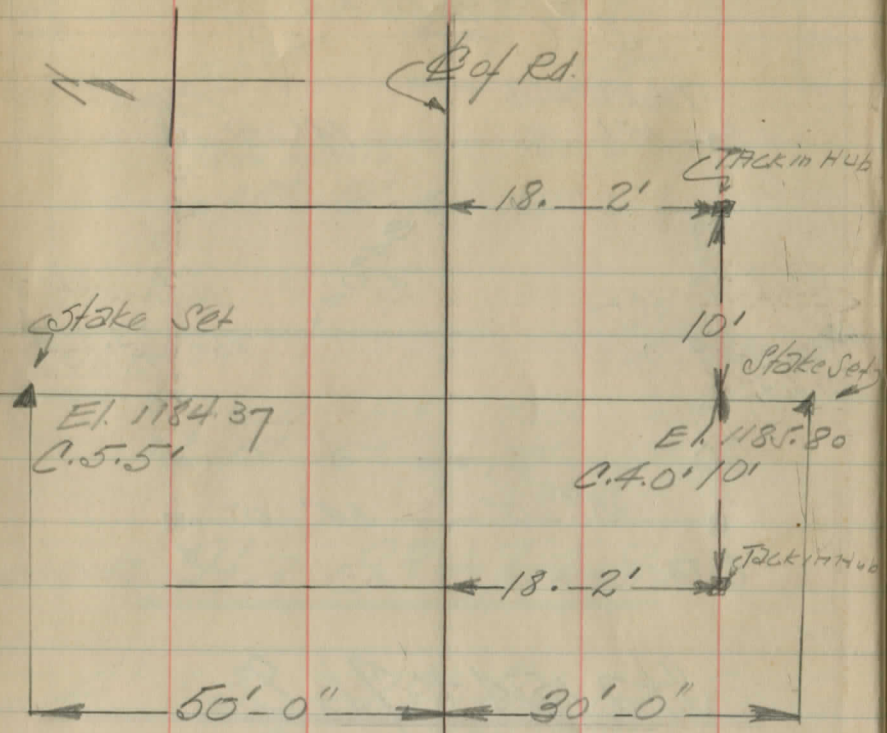


Sta 104+71.8

4' x 3' x 27' Slab Top Ext.
 Hubs with Tacks set on 1' offset

S. Gold Jr.
 S. Merritt
 H. Barton

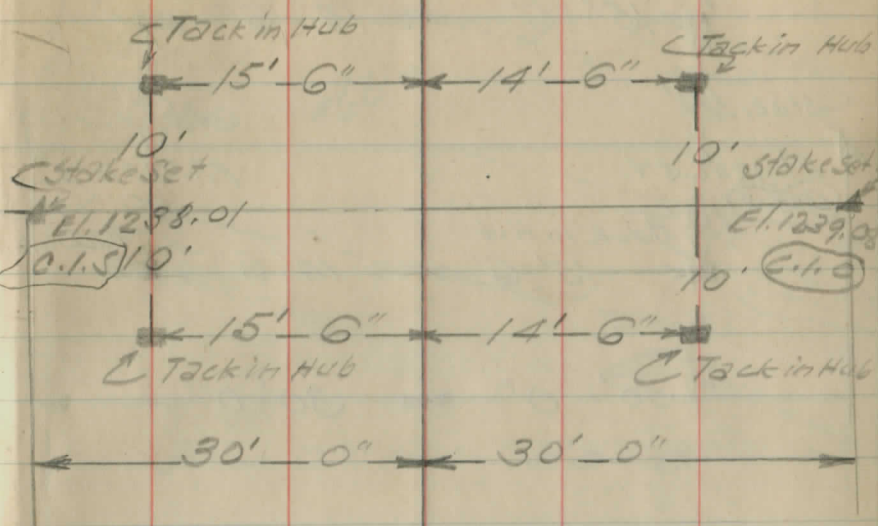
Wilson's Corners N. S Gold Jr
 Oct 14-29 Fair S Merritt



Sta 178+08.1

4' x 4' x 8' Conc. Slab Top
 Culvert Extension
 Hubs with tack on S. Side set on
 5' offset.

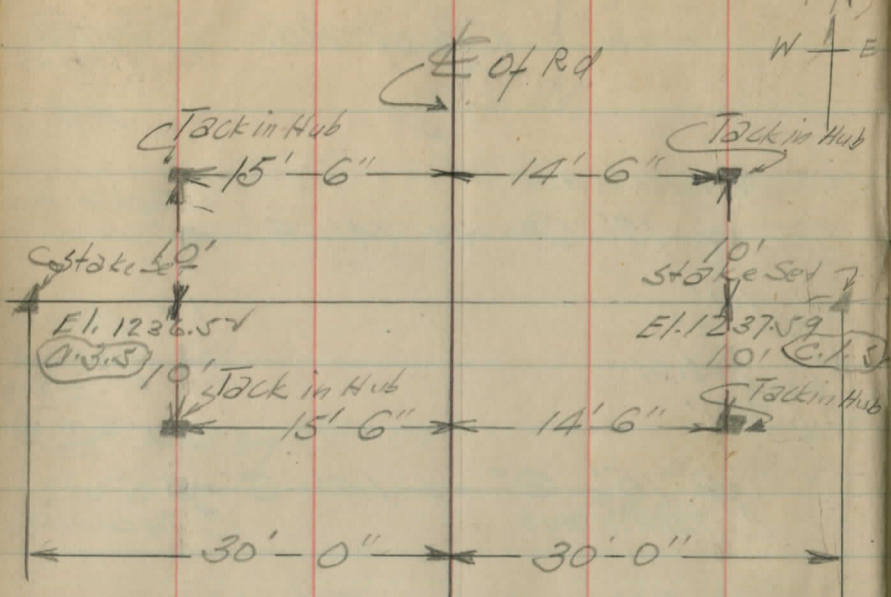
Wilson's Corners N. 10-19-29 69
 S Gold Jr
 S Merritt



Sta 32+18

15" x 28' C.I.P.
 Hubs with Tacks set on 1' offset

Wilson's Corners



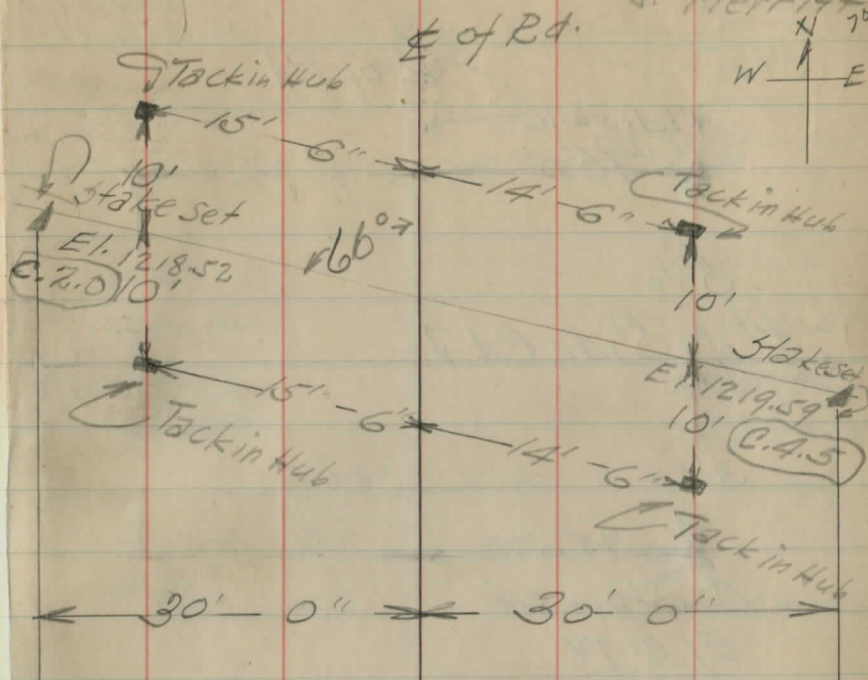
Sta 35+54

18" x 28' C.I.P. Culvert

Hubs with Tacks set on 1' offset

10-21-79

S. Gold Jr
S. Merritt

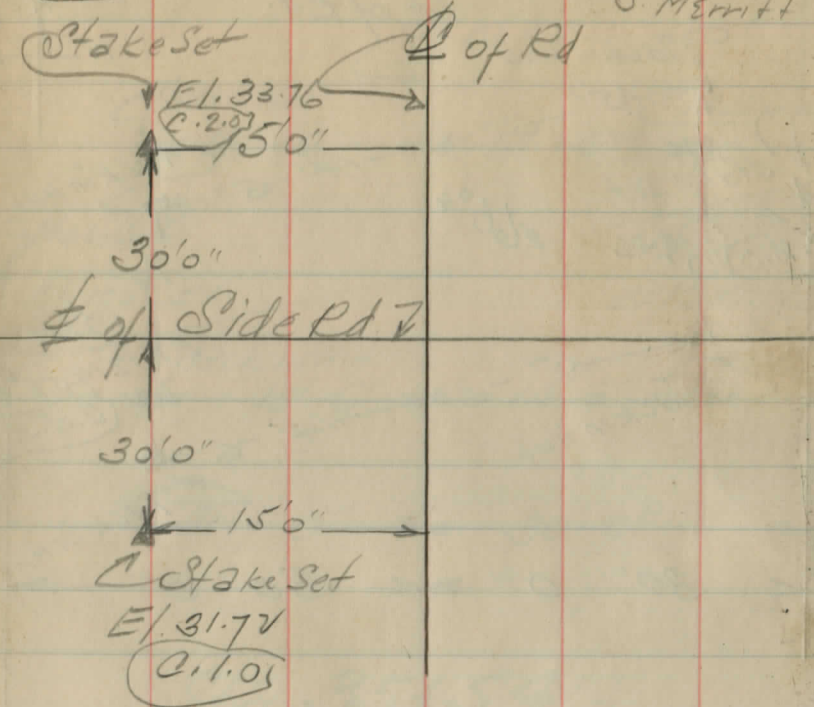


Sta 69+55

C.I.P.
18" x 28' Hillside Culvert

Hubs with Tacks set on 1' offset

Rain Wilson's Farmers N. 10-22-29
 S Gold Fr
 S Merritt

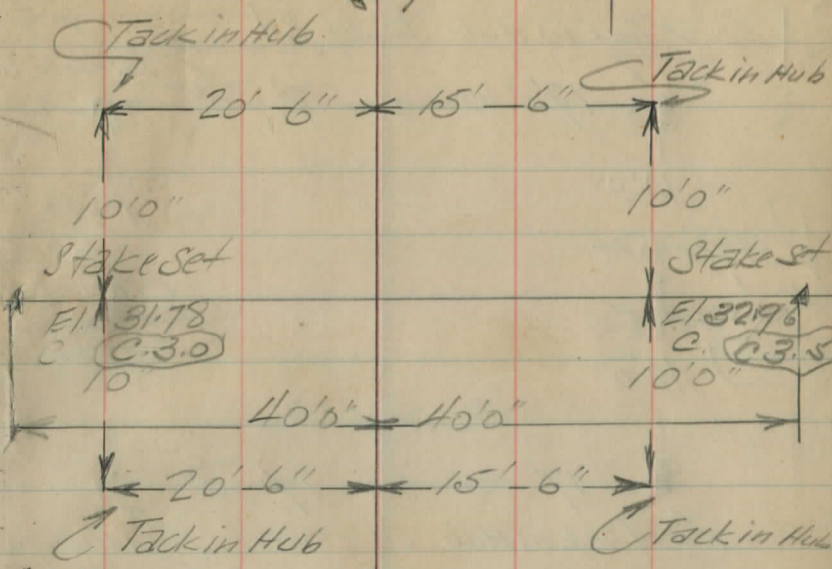


Hubs with Tacks Set on 1' offset

Sta 125+37

15" C.I.P. Side Rd. Pulvert

10-25-29 Wilson's Farmers North S Gold Fr
 S Merritt 71
 Fair



Sta 138+71±

Hubs with Tack Set on 1' offset

Rd Ditches to be Deepened

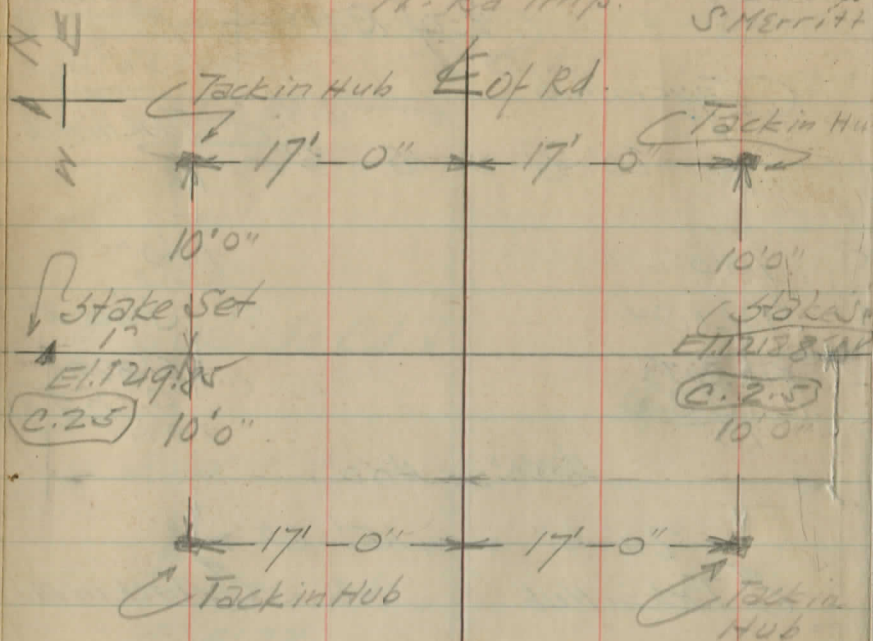
150' South of Pulvert

Open Outlet Channel 150'

Flow Line Elev. shown on Plans

Changed to meet the depth of Existing Ditches

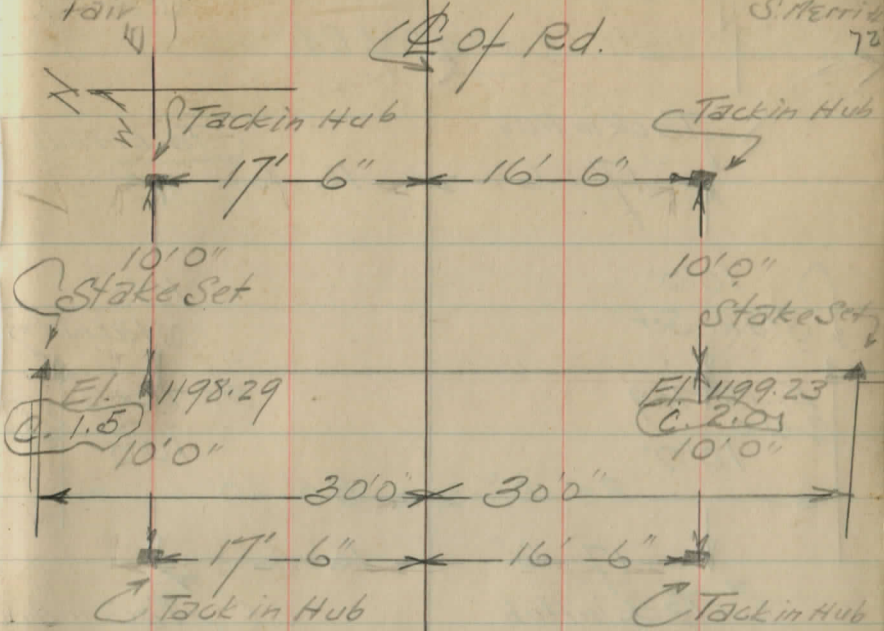
Wilson's Corners 10-25-29
 N. Rd Imp. S Gold 30
 S Merritt



Sta 154+17

Hubs with Tacks Set on 2' offset
 Open outlet channel for 300'
 Reduce the 32' pipe to 30'
 & Change the Hillside culvert
 to a regular type of a culvert
 with Standard Headwalls. The 1.1 cu yd.
 of concrete to be deducted from
 the Extra Work Estimate S.G.

10-26-29 Wilson's Corners North S Gold
 Fair S Merritt 72



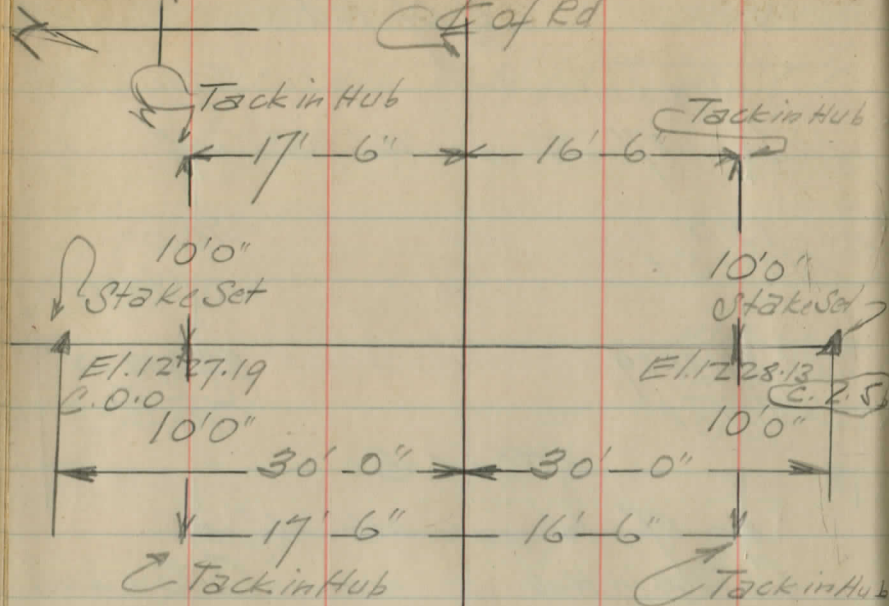
Sta 183+90

18" Corr Iron Pipe
 Hubs with Tacks Set on 1' offset

Oct 26-29 Wilson's Corners North
Fair

S. Gold St.
S. Merritt

Ct of Rd



Sta 193+17

Hubs with Tacks Set on 1' offset

April 6, 1957

Levels Messenger Rd.
1350' S. of Franks RdCloudy - Snow
30°H. Patterson
D. Canfield

74

Sta	+ H.I.	- Elev
B.M.	4.26	104.26
0+0		8.90
100		100.00
200		
300		
400		
T.P.	6.22	101.58
500		6.25
600		95.36
T.P.	8.51	103.84
B.M.		3.90
		95.33
		99.94

Horz	S.P.K. W side C.E.I. E. side Rd	# 596315 # 268932
6" Drain tile Flo-E.	W Ditch 98.86 5.40	E Ditch 98.51 5.75
	98.38	97.94
	5.88	6.22
	97.24	96.81
	6.92	7.35
	96.31	95.96
	7.95	8.30
	95.21	95.26
	9.05	9.00
	94.68	94.48
	6.90	7.10
Flo-W. Culvt. 35x3' conc. Box	93.28	93.28
	8.30	8.30

5.2

H. Patterson 6/4/1974 Level 1350's. of Franks
 R. Eging Messenger Rd

	+	M	-	Elev.
B.M.	3.91	103.91		100.00

0+0

+50 Dr. way west 12' conc.

1+00

2+00

3+00

4+00

5+00

6+00

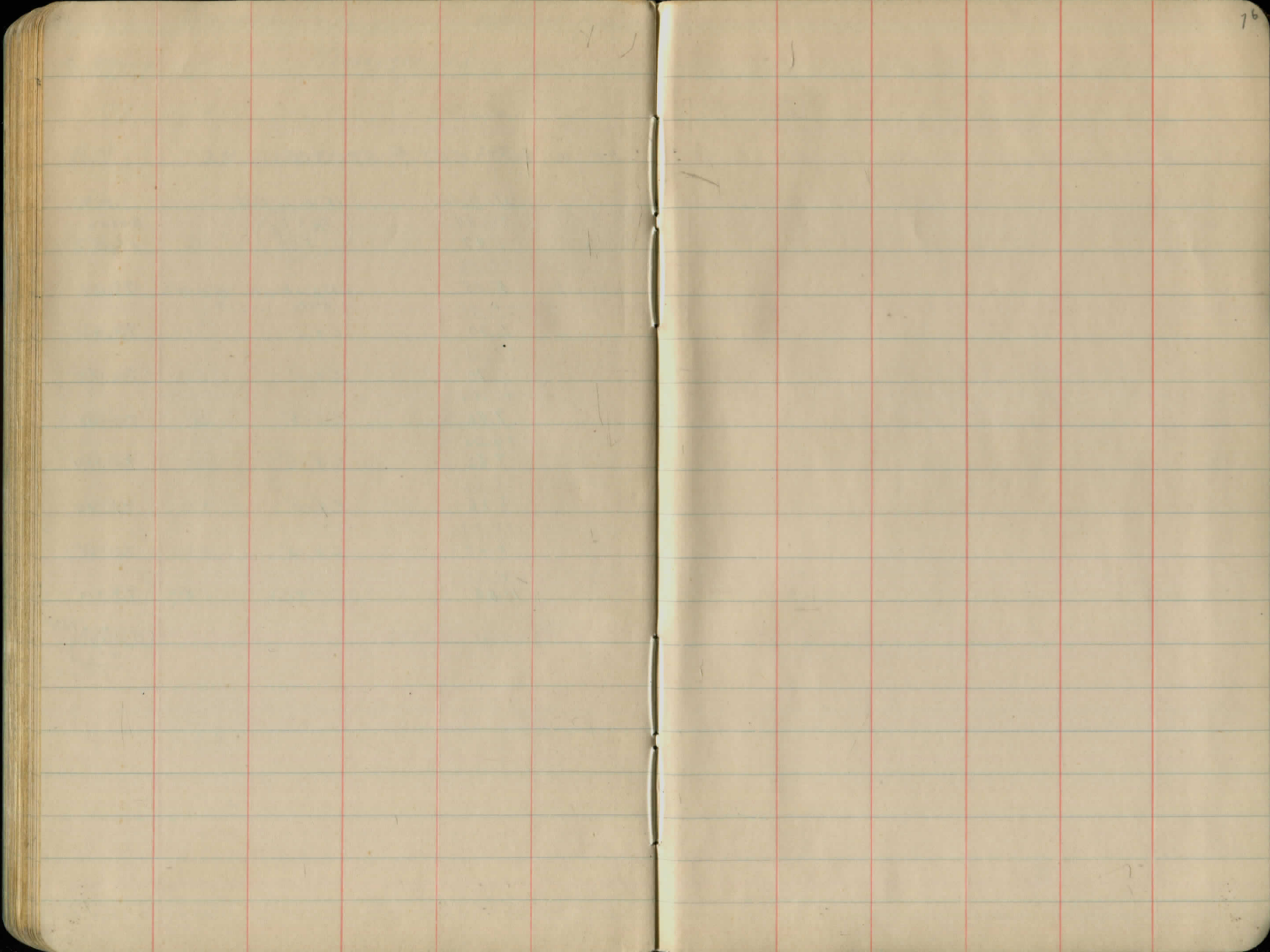
+75 F/L Slab Culvert

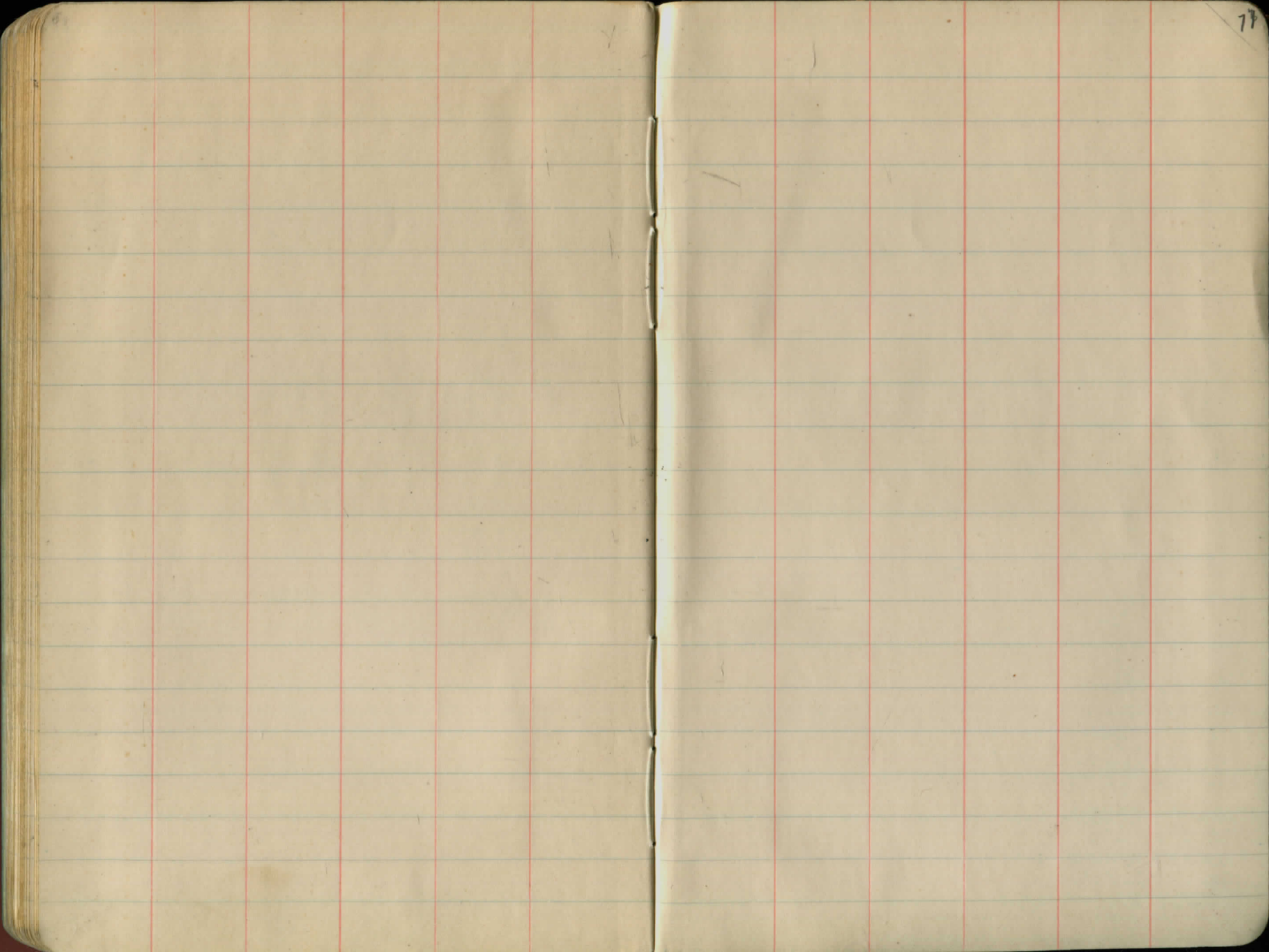
B.M.		3.91		100.00
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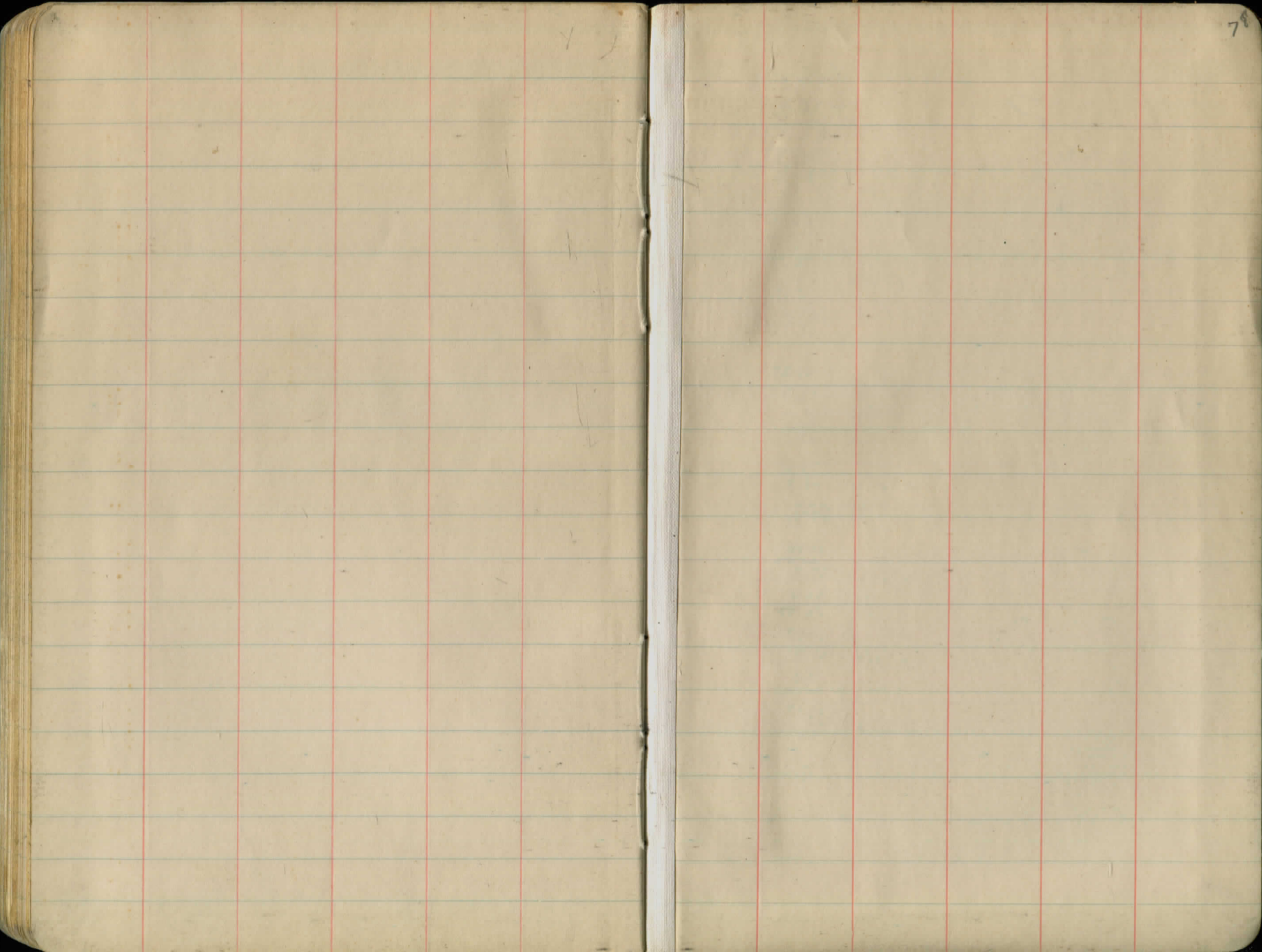
SPR W. side CET # 596315

	W. Ditch	10' W. in field	180%
H/4" Tile	98.44	F/4" Tile 96.38 5.53	Grade
W. side	5.47		Elev.
	98.46		
Inlet end	5.45	Top of stake	.40 98.04
	97.71		
	6.20	C 4'-6"	.8 97.64
	97.21		
	6.70	C 4'-0"	1.6 96.84
	96.45		
	7.46	C 5'-6"	2.4 96.04
	96.05		
	7.86	C 3'-6"	3.2 95.24
	95.65		
	8.26	C 4'-0"	4.0 94.44
	95.23		
	8.68	C 4'-0"	4.8 93.64
	93.11		
	10.80		5.8 93.14

985
 675 530.0
 475
 5850







103.91
 4.33

 99.58
 97.64

 1.94

1.60

 102.31 1.77
 97.64

 4.67 4'-6" C

2.20

 101.21

96.84 3.07 4'-00" C
 4.37

2.01

 101.90

96.04
 3.86 5'-6" C

 4.92 (5.17)
 98.99

95.24
 3.75 5'-6" C

5.05 (5.47)

 98.52

94.44
 4.12 4'-0" C

 6.20

97.61
 93.64

 4.00 4'-00" C

U-
 3'-0"
 3'-6"

70

TABLE IX.—CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.44	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w=16.2$ and $h=5.3$, cu. yds. $=1.48+.028+.089=1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $=h$, and $\frac{1}{2}$ the roadbed $=w$, add the triangles formed by taking the distance out to each break in turn ($=w$'s) by the difference between the cuts (or fills) on each side of it ($=h$'s) always subtracting the outer from the inner.

PLEASE RETURN TO
 DISTANCE FROM CENTER OF ROADWAY FOR
 CROSS SECTIONING.
 GEAUGA COUNTY ENGINEER
 Roadway 16 feet wide. Side Slopes 1 on 1 1/2.
 for Single Track Embankment.
 CHARDON, O.
 PHONE 250-X

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9+(20-16)+2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

